# Learning Constitutive Models in Multiscale Modeling of Materials

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## Outline

- Problem Statement
- Methodology
- Numerical Examples
- Conclusion & Outlook

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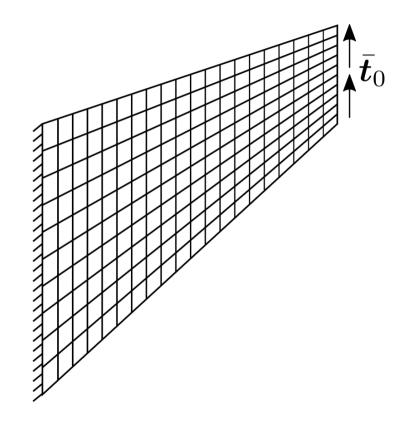
#### **Problem Statement**

 $\begin{aligned} & \text{Macroscopic Problem: Find } \bar{\boldsymbol{u}}(\bar{\boldsymbol{X}}) \\ & \text{Div} \bar{\boldsymbol{P}}(\bar{\boldsymbol{u}}) = \boldsymbol{0} & \text{on } \bar{\Omega}, \\ & \bar{\boldsymbol{P}} \bar{\boldsymbol{N}} = \bar{\boldsymbol{t}}_0 & \text{on } \partial \bar{\Omega}^N, \\ & \bar{\boldsymbol{u}} = \bar{\boldsymbol{u}}_0 & \text{on } \partial \bar{\Omega}^D, \end{aligned}$ 

**Constitutive Model** 

$$ar{m{P}} = ar{m{P}}(ar{m{F}},m{\mu}) \ ar{m{F}} = m{I} + rac{\partialar{m{u}}}{\partialar{m{X}}} \ ar{m{A}} = rac{\partialar{m{P}}(ar{m{F}},m{\mu})}{\partialar{m{F}}}$$

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[Guo, T., Rokoš, O., and Veroy, K., 2021, CMAME 384]

#### **Problem Statement**

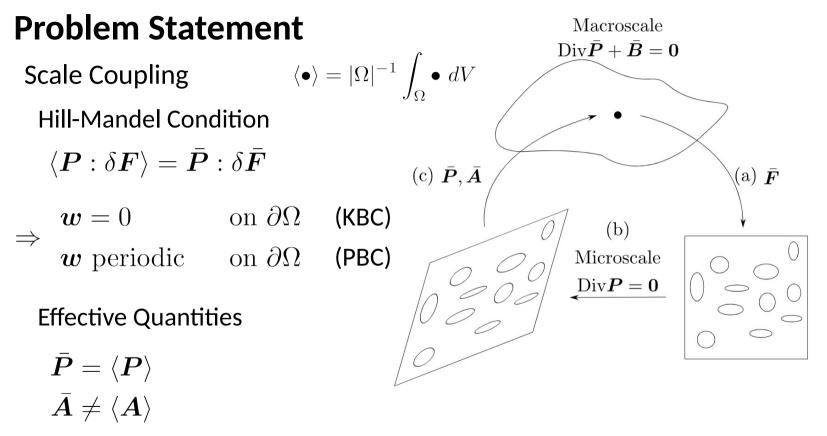
Microscopic Problem: Find  $oldsymbol{u}(oldsymbol{X})$ 

Div
$$P(u) = 0$$
 on  $\Omega$   
 $u = \underbrace{(\bar{F} - I)X}_{\text{mean}} + \underbrace{w(X)}_{\text{fluctuation}}$ 

Neo-Hookean material

$$\begin{split} W(\boldsymbol{F},\boldsymbol{\mu}) &= C_1(\mathrm{Tr}(\boldsymbol{F}^T\boldsymbol{F}) - 3 - 2\ln(\det\boldsymbol{F})) + D_1(\det\boldsymbol{F} - 1)^2 \\ \boldsymbol{P}(\boldsymbol{F},\boldsymbol{\mu}) &= \frac{\partial W}{\partial \boldsymbol{F}} & \bar{\boldsymbol{F}} \text{ loading: macroscopic deformation gradient} \\ \boldsymbol{A}(\boldsymbol{F},\boldsymbol{\mu}) &= \frac{\partial \boldsymbol{P}}{\partial \boldsymbol{F}} & \mu \text{ parameters: material \& geometry} \\ \end{split}$$

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[Guo, T., Rokoš, O., and Veroy, K., 2021, CMAME 384]

#### **Problem Statement**

- Full two-scale simulations → too expensive (multi-query contexts: optimization, materials design, etc.)
- Non-intrusive and accurate approximation of the microscopic stress field for different parameters
- Obtain rapidly effective stress  $\rightarrow$  reducing to a single-scale problem

$$oldsymbol{P}(oldsymbol{X},ar{oldsymbol{F}},oldsymbol{\mu}),\quadar{oldsymbol{P}}(ar{oldsymbol{F}},oldsymbol{\mu})$$

- Accurate effective stiffness and sensitivities

$$ar{m{A}} = rac{\partialar{m{P}}(ar{m{F}},m{\mu})}{\partialar{m{F}}}, \quad rac{\partialar{m{P}}(ar{m{F}},m{\mu})}{\partialm{\mu}}$$

#### Intrusive RB Method

Approximate displacement field

[Yvonnet, J. and He, Q.C., 2007, JCP 223] [Radermacher, A., et al., 2016, AMSES 3(1)] [Hernández, J. A., et al., 2014, CMAME 276] [Soldner, Dominic, et al., 2017, Comput. Mech. 60(4)]

 $m{u}(m{X},ar{m{F}},m{\mu}) pprox \sum_{l=1}^{L} lpha_l(ar{m{F}},m{\mu}) m{\Phi}_l(m{X}) = m{\Phi}m{lpha}$  with  $\ m{\Phi}(m{X})$  RB basis functions

Reduced problem

$$f(\Phi\alpha) = 0$$
Need hyperreduction!
$$\Phi^T Df|_{\Phi\alpha^k} \Phi\Delta\alpha = -\Phi^T f(\Phi\alpha^k)$$

$$\alpha^{k+1} = \alpha^k + \Delta\alpha$$

- Hyperreduction (convergence problems)
- Intrusive (requires access to the microscopic solver)

#### Non-Intrusive RB Method

Approximate displacement field

[Guo, M. and Hesthaven, J.S., 2018, CMAME 341] [Kast, M., Guo, M. and Hesthaven, J.S., 2020, CMAME 364] [Swischuk, Renee, et al., 2019, Comput Fluids 179]

$$m{u}(m{X},ar{m{F}},m{\mu})pprox \sum_{l=1}^{L}lpha_l(ar{m{F}},m{\mu}) \Phi_l(m{X}) = m{\Phi}m{lpha}$$
 with  $\ m{\Phi}(m{X})$  RB basis functions

Instead of solving reduced system, perform a regression to obtain

 $\hat{\alpha}_l: \mathcal{P} \to \mathbb{R}: (\bar{F}, \mu) \mapsto \hat{\alpha}_l(\bar{F}, \mu)$ 

For a new pair  $(\bar{F}, \mu)$ , the coefficients  $\alpha$  can be directly obtained



#### Non-Intrusive RB Method

Approximate displacement field

[Guo, M. and Hesthaven, J.S., 2018, CMAME 341] [Kast, M., Guo, M. and Hesthaven, J.S., 2020, CMAME 364] [Swischuk, Renee, et al., 2019, Comput Fluids 179]

$$m{u}(m{X},ar{m{F}},m{\mu})pprox\sum_{l=1}^Llpha_l(ar{m{F}},m{\mu}) \Phi_l(m{X}) = m{\Phi}m{lpha}$$
 with  $\ m{\Phi}(m{X})$  RB basis functions

To obtain stresses, gradient of u is needed, and evaluation of the constitutive model

- Intrusive: Need to implement material model
- **Slow**: Need to evaluate material model  $N_{\rm qp}$  times

Idea: Approximate stress field directly!  
$$P(X, \bar{F}, \mu) \approx \sum_{l=1}^{L} \alpha_l(\bar{F}, \mu) B_l(X)$$

Proper Orthogonal Decomposition (POD)

1. Collect stress snapshots

$$\mathbf{S} = \begin{bmatrix} \mathbf{P}^{(1)}, \mathbf{P}^{(2)}, \dots, \mathbf{P}^{(N_{\text{pod}})} \end{bmatrix}$$

2. Compute correlation matrix

$$C_{ij} = \left(\boldsymbol{P}^{(i)}, \boldsymbol{P}^{(j)}\right)_{L^2(\Omega)} = \int_{\Omega} \boldsymbol{P}^{(i)} : \boldsymbol{P}^{(j)} dV$$

- 3. Compute the eigenvalues  $\lambda_l$  and eigenvectors  $\mathbf{v}_l$  of  $\mathbf{C}$
- 4. Compute the basis functions

$$\begin{split} \mathbf{B}_{l} &= \frac{1}{\sqrt{\lambda_{l}}} \mathbf{S} \mathbf{v}_{l} \\ \Rightarrow \mathbf{P}^{\mathrm{RB}}(\mathbf{X}, \bar{\mathbf{F}}, \boldsymbol{\mu}) &= \sum_{l=1}^{L} \alpha_{l}(\bar{\mathbf{F}}, \boldsymbol{\mu}) \mathbf{B}_{l}(\mathbf{X}) \\ &= \sum_{l=1}^{L} \alpha_{l}(\bar{\mathbf{F}}, \boldsymbol{\mu}) \mathbf{B}_{l}(\mathbf{X}) \end{split}$$

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[Guo, T., Rokoš, O., and Veroy, K., 2021, CMAME 384]

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MethodologyEffective Quantities
$$\bar{P} = \langle P^{\text{RB}} \rangle = |\Omega|^{-1} \int_{\Omega} P^{\text{RB}} dV = |\Omega|^{-1} \sum_{l=1}^{L} \alpha_l(\bar{F}, \mu) \int_{\Omega} B_l(X) dV$$
 $\bar{A} = \frac{\partial \bar{P}}{\partial \bar{F}} = |\Omega|^{-1} \sum_{l=1}^{L} \int_{\Omega} B_l(X) dV \otimes \frac{\partial \alpha_l(\bar{F}, \mu)}{\partial \bar{F}}$ Sensitivities $\frac{\partial \bar{P}}{\partial \mu} = |\Omega|^{-1} \sum_{l=1}^{L} \int_{\Omega} B_l(X) dV \otimes \frac{\partial \alpha_l(\bar{F}, \mu)}{\partial \mu}$  $\Rightarrow$  Construct  $\hat{\alpha}_l(\bar{F}, \mu), \frac{\partial \hat{\alpha}_l(\bar{F}, \mu)}{\partial \bar{F}}, \frac{\partial \hat{\alpha}_l(\bar{F}, \mu)}{\partial \bar{F}}$  with Gaussian Process Regression!

#### Gaussian Process Regression (GPR)

Given some data  $\{\mathbf{X}^{(i)}, y^{(i)}\}_{i=1}^{N}$ , we want to find a scalar regression function which is distributed as a Gaussian Process with zero mean function and kernel  $k_{\theta}(\mathbf{X}, \mathbf{X}')$ 

 $f \sim \mathcal{GP}(0, k_{\theta}(\mathbf{X}, \mathbf{X}'))$ 

Automatic relevance determination (ARD) squared exponential kernel

$$k_{\boldsymbol{\theta}}(\mathbf{X}, \mathbf{X}') = \sigma_f^2 \exp\left(-\frac{1}{2} \sum_{k=1}^d \frac{(X_k - X_k')^2}{l_k^2}\right)$$



#### Gaussian Process Regression (GPR)

Given some data  $\{\mathbf{X}^{(i)}, y^{(i)}\}_{i=1}^{N}$ , we want to find a scalar regression function which is distributed as a Gaussian Process with zero mean function and kernel  $k_{\theta}(\mathbf{X}, \mathbf{X}')$ 

$$f^*|(\mathbf{X}, \mathbf{y}) \sim \mathcal{GP}(m^*, k^*),$$
  

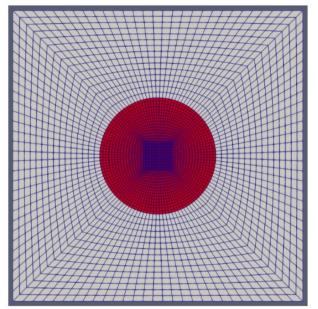
$$m^*(\mathbf{x}) = \mathbf{k}_{\theta}(\mathbf{X}, \mathbf{x})^T \mathbf{k}_{\theta}(\mathbf{X}, \mathbf{X})^{-1} \mathbf{y}(\mathbf{X}),$$
  

$$k^*(\mathbf{x}, \mathbf{x}') = k_{\theta}(\mathbf{x}, \mathbf{x}') - \mathbf{k}_{\theta}(\mathbf{X}, \mathbf{x})^T \mathbf{k}_{\theta}(\mathbf{X}, \mathbf{X})^{-1} \mathbf{k}_{\theta}(\mathbf{X}, \mathbf{x}')$$

where 
$$\mathbf{k}_{\theta}(\mathbf{X}, \mathbf{x}) = [k_{\theta}(\mathbf{X}^{(1)}, \mathbf{x}), k_{\theta}(\mathbf{X}^{(2)}, \mathbf{x}), \dots, k_{\theta}(\mathbf{X}^{(N)}, \mathbf{x})]^T$$
  
 $\mathbf{k}_{\theta}(\mathbf{X}, \mathbf{X}) = [k_{\theta}(\mathbf{X}^{(i)}, \mathbf{X}^{(j)})]_{i,j=1}^N$   
 $\mathbf{y}(\mathbf{X}) = [f(\mathbf{X}^{(1)}), f(\mathbf{X}^{(2)}), \dots, f(\mathbf{X}^{(N)})]^T$ 

#### Fiber reinforced microstructure

- 4321 eight-node elements with 4 quadrature points
- Volume fraction of fiber is 12.56%
- Matrix material  $C_1^{\mathrm{mat}} = D_1^{\mathrm{mat}} = 1$
- Fiber material  $C_1^{\mathrm{fib}} = D_1^{\mathrm{fib}} \in [50, 150]$
- Deformations  $ar{oldsymbol{U}} \mathbf{I} \in [-0.3, 0.3]$
- 500 training snapshots (Sobol sequence)
- 1000 testing snapshots (uniformly random)
  - $\begin{array}{c} \mathbf{P}\text{-PODGPR}\,\bar{\mathbf{E}}\text{rror}\\ \epsilon_{\bar{\mathbf{P}}} \coloneqq \frac{\left\|\bar{\mathbf{P}}^{\mathrm{HF}} \bar{\hat{\mathbf{P}}}^{\mathrm{RB}}\right\|_{\mathrm{F}}}{\left\|\bar{\mathbf{P}}^{\mathrm{HF}}\right\|_{\mathrm{F}}} \end{array}$
- Projection Error  $\epsilon_{\bar{\mathbf{P}}} \coloneqq \frac{\|\bar{\mathbf{P}}^{\mathrm{HF}} - \bar{\mathbf{P}}^{\mathrm{RB}}\|_{\mathrm{F}}}{\|\bar{\mathbf{P}}^{\mathrm{HF}}\|_{\mathrm{F}}}$



$$W(\boldsymbol{F}, \boldsymbol{\mu}) = C_1(\operatorname{Tr}(\boldsymbol{F}^T \boldsymbol{F}) - 3 - 2\ln(\det \boldsymbol{F})) + D_1(\det \boldsymbol{F} - 1)^2$$

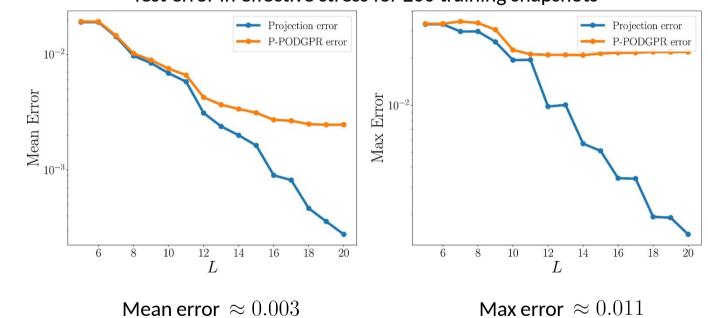
#### Fiber reinforced microstructure

 $10^{4}$ 20 snapshots 50 snapshots  $10^{1}$ 100 snapshots  $10^{-2}$  t 200 snapshots Eigenvalue 500 snapshots  $10^{-5}$ 1000 snapshots  $10^{-8}$  $10^{-11}$  $10^{-14}$ 200 400 600 800 1000 0 L With L = 20,  $\frac{\sum_{i=1}^{L} \lambda_i}{\sum_{i=1}^{N} \lambda_i} = 0.9999$ 

POD for different numbers of training snapshots

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Fiber reinforced microstructure

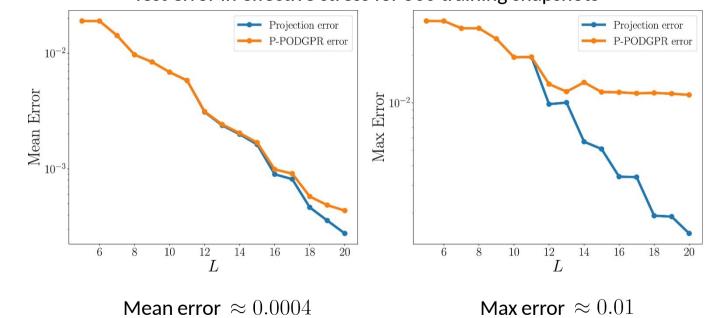


Test error in effective stress for 200 training snapshots

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Fiber reinforced microstructure



Test error in effective stress for 500 training snapshots

#### Fiber reinforced microstructure

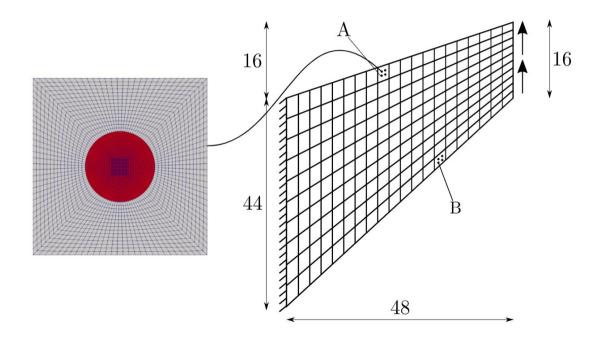
- Comparison with a neural network (Multilayer Perceptron) that is trained with pairs of  $\{\bar{U}^{(i)}, \bar{P}^{(i)}\}_{i=1}^{N}$  with N = 500 training snapshots
- Trained with Adam optimizer with learning rate of  $10^{-4}$ , batch size of 32 and Mean Squared Error Loss function for different architectures
- ELU activation function was applied after every layer apart from last layer

Architecture	Validation Loss	$\epsilon_{ar{\mathbf{P}}}^{\mathrm{mean}}$	$\epsilon_{ar{\mathbf{P}}}^{\max}$
$N_h = 1, N_n = 20$	$1.7 \times 10^{-6}$	0.0077	0.0368
$N_h = 1, N_n = 50$	$8.55 \times 10^{-7}$	0.0056	0.0289
$N_h = 2, N_n = 20$	$5.36 \times 10^{-7}$	0.0047	0.0176
$N_h = 2, N_n = 50$	$2.97 imes10^{-7}$	0.0039	0.0206
$N_h = 2, N_n = 100$	$7.91 \times 10^{-7}$	0.0052	0.0315

⇒ P-PODGPR outperforms all neural networks, while also being able to recover the microscopic stress field

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Two-scale Cook's membrane problem

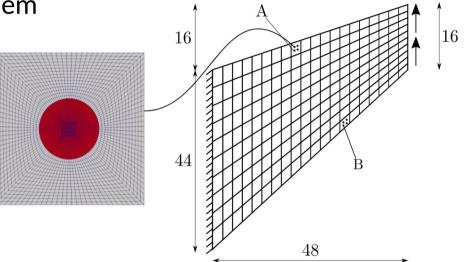


#### Two-scale Cook's membrane problem

- 200 four-node elements with 4 quadrature points
- Vertical traction of 0.1 on right edge
- Left edge is fixed
- Matrix material  $C_1^{\text{mat}} = D_1^{\text{mat}} = 1$
- Fiber material  $C_1^{\overline{fib}} = D_1^{\overline{fib}} = 100$
- Surrogate model trained with 200 snapshots
- Relative error to compare microscopic stresses

$$\epsilon_{P_{yx}} \coloneqq |P_{yx}^{\text{FE2}} - P_{yx}^{\text{ROM}}| / \left\langle |P_{yx}^{\text{FE2}}| \right\rangle$$

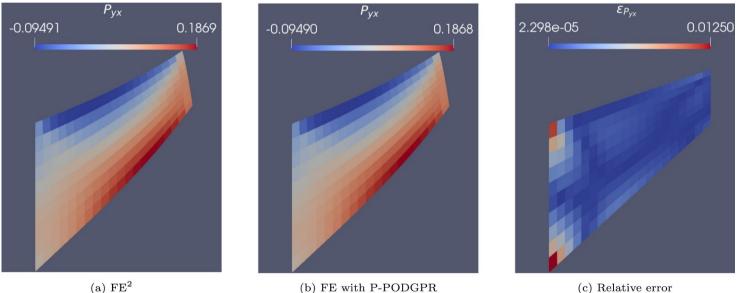
 $\left< |P_{yx}^{ ext{FE2}}| 
ight>$ : Averaged absolute stress



$$W(\boldsymbol{F}, \boldsymbol{\mu}) = C_1(\operatorname{Tr}(\boldsymbol{F}^T \boldsymbol{F}) - 3 - 2\ln(\det \boldsymbol{F})) + D_1(\det \boldsymbol{F} - 1)^2$$

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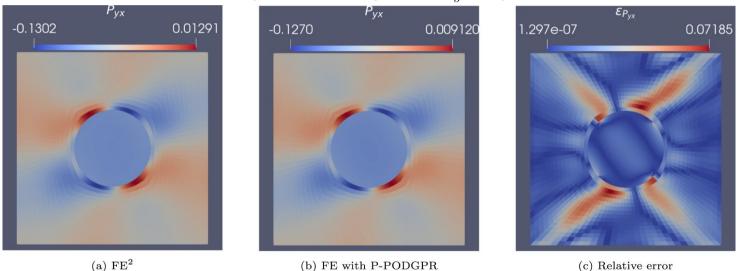
#### Two-scale Cook's membrane problem



#### Macroscopic stress component $P_{yx}$

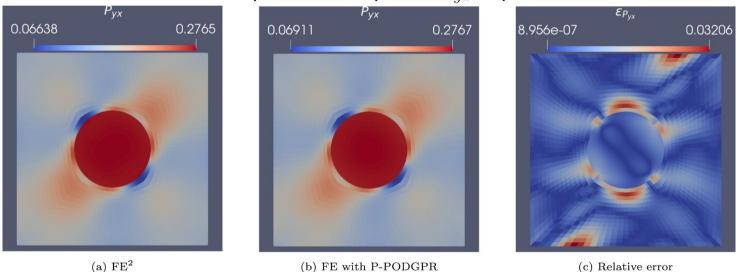
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Two-scale Cook's membrane problem



Microscopic stress component  $P_{yx}$  at point A

#### Two-scale Cook's membrane problem



#### Microscopic stress component $P_{yx}$ at point B

#### Two-scale Cook's membrane problem

	FE <sup>2</sup>	FE with P-PODGPR
Snapshot generation	-	$60 \min$
POD + GPR	_	$1 \min$
Online simulation	$4800 \min$	$1 \min$

 $\Rightarrow$  Online speedup of the order of 1000

### **Conclusion & Outlook**

#### Summary

- Novel method based on non-intrusive reduced basis method
- Validated on 2D composite microstructure and multiscale application
- High accuracy and online speedup
- Sensitivities are available and can be used for optimization

#### Outlook

- Geometrical parameters
- Dissipative constitutive models (Plasticity, Damage)
- Test on 3D problems

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