



Development of 1D2D3D flow solver D-FLOW Flexible Mesh

3TU.AMI, 13-11-2014

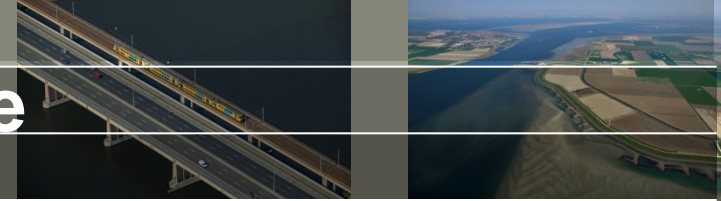
Herman Kernkamp, Sander v/d Pijl, Arthur v. Dam,
Guus Stelling

Deltares: Water & Soil

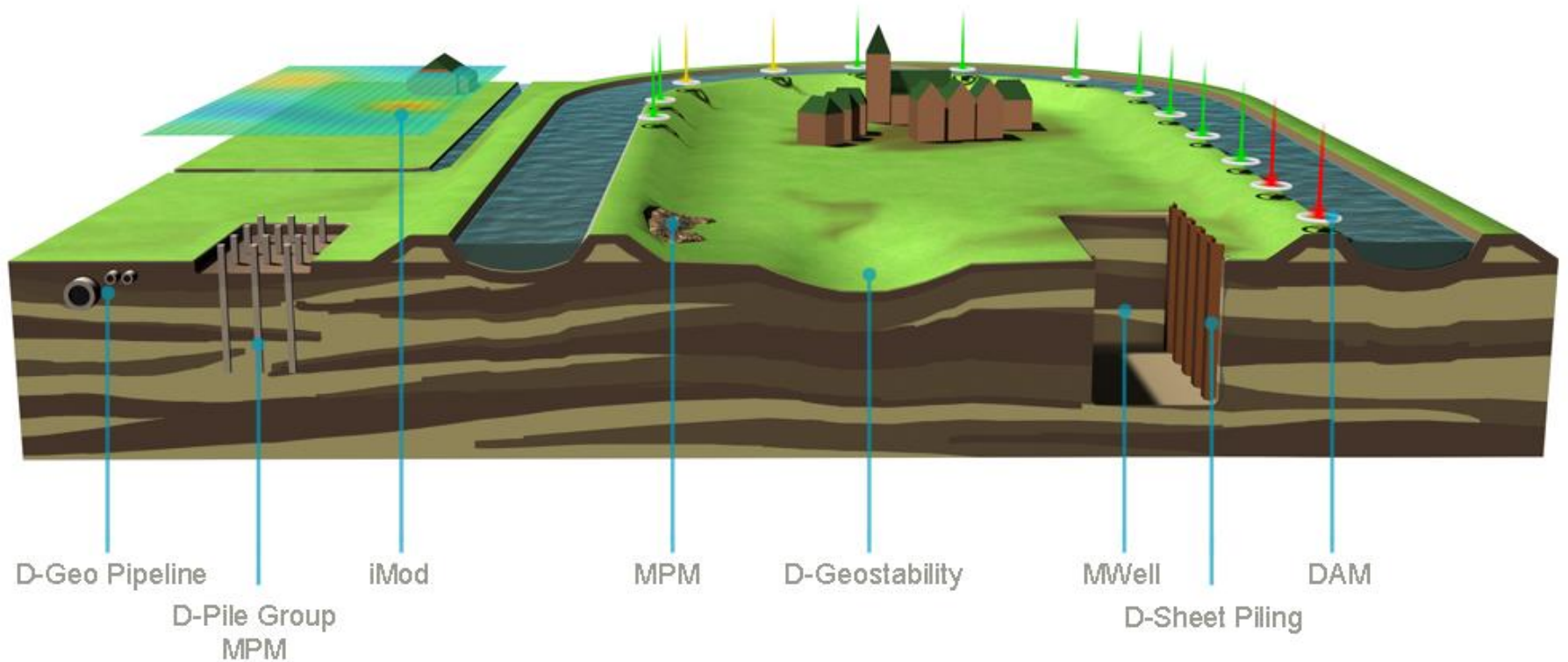
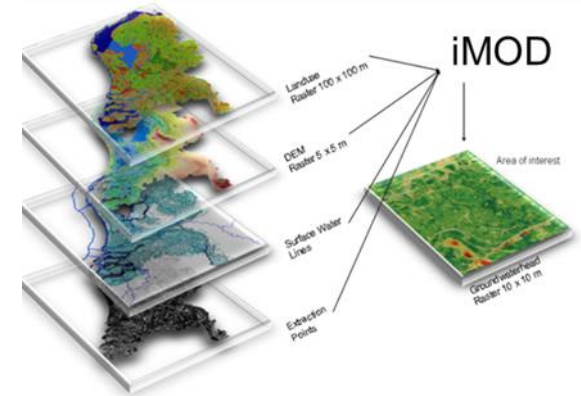
Delft & Utrecht 800



Next Generation Geo Software



NEXT GENERATION GEO SOFTWARE



Next Generation Hydro Software



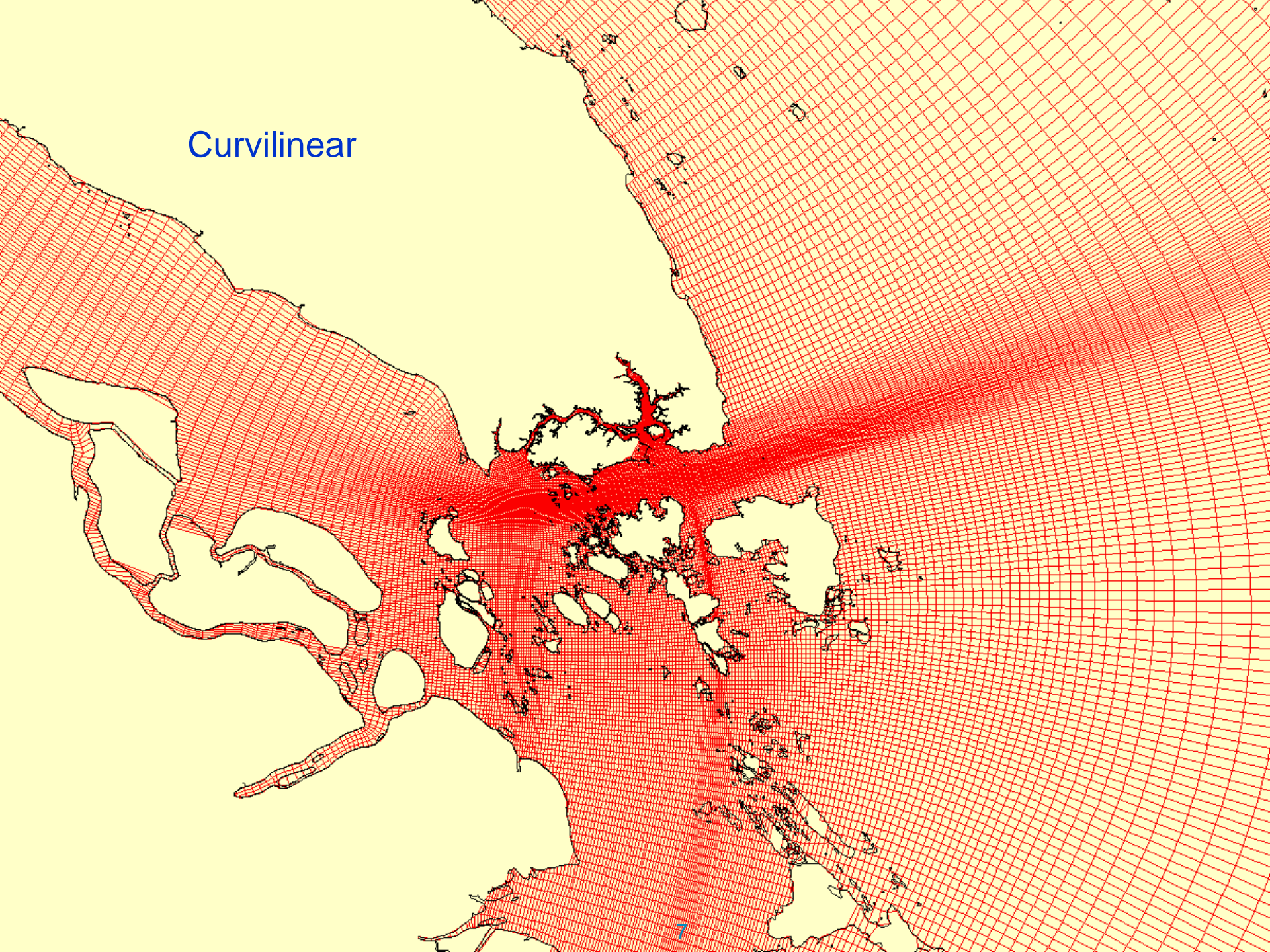
Sobek1D-2D



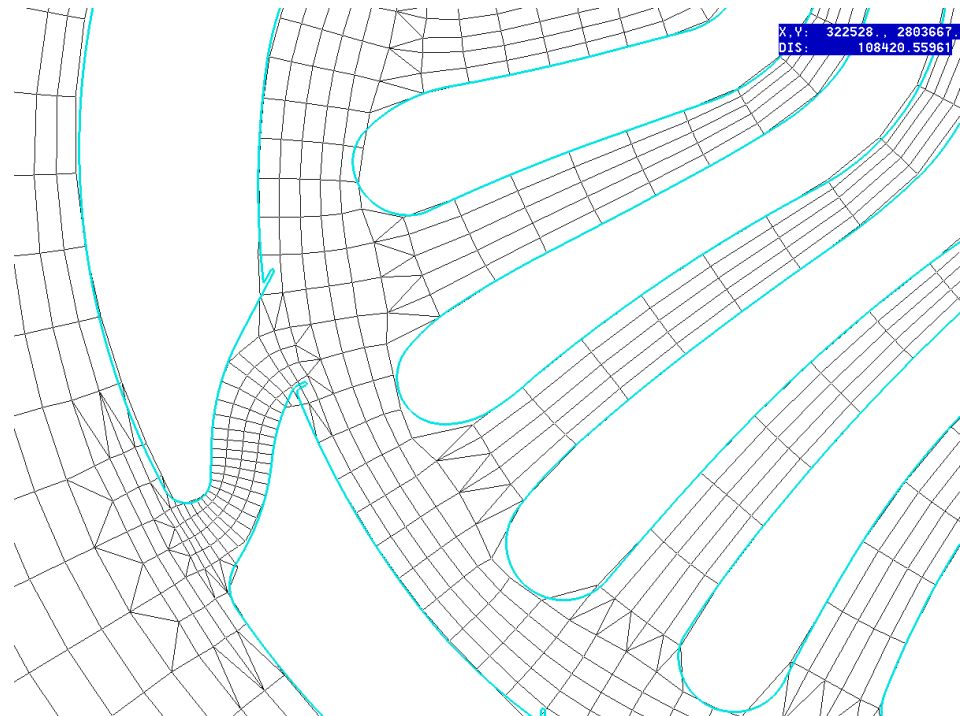
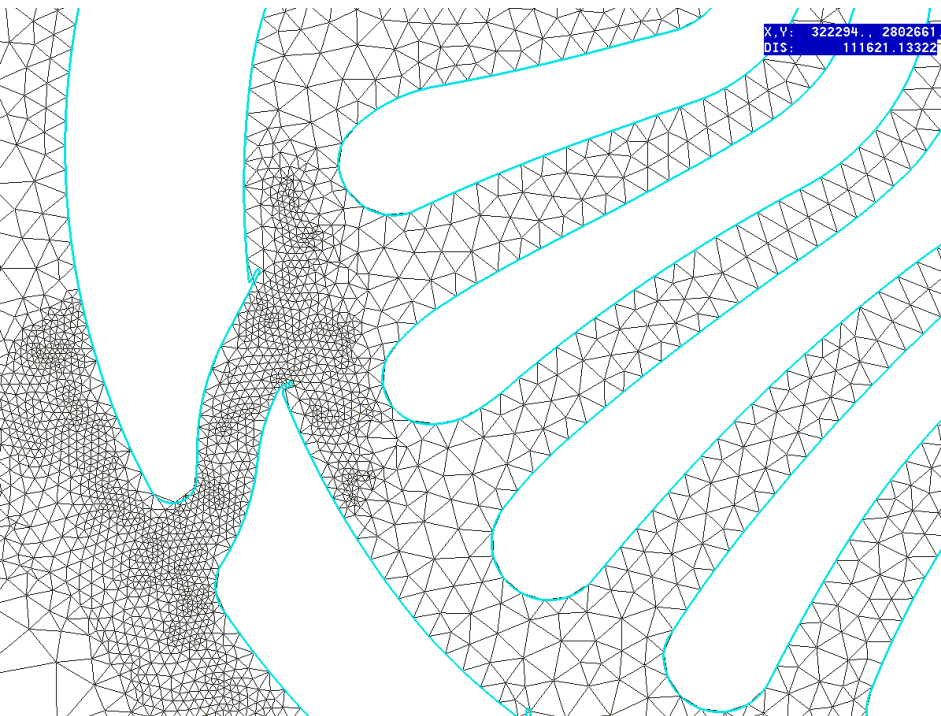
Delft-3D



Curvilinear



Flexibility : Curvilinear + occasional triangle



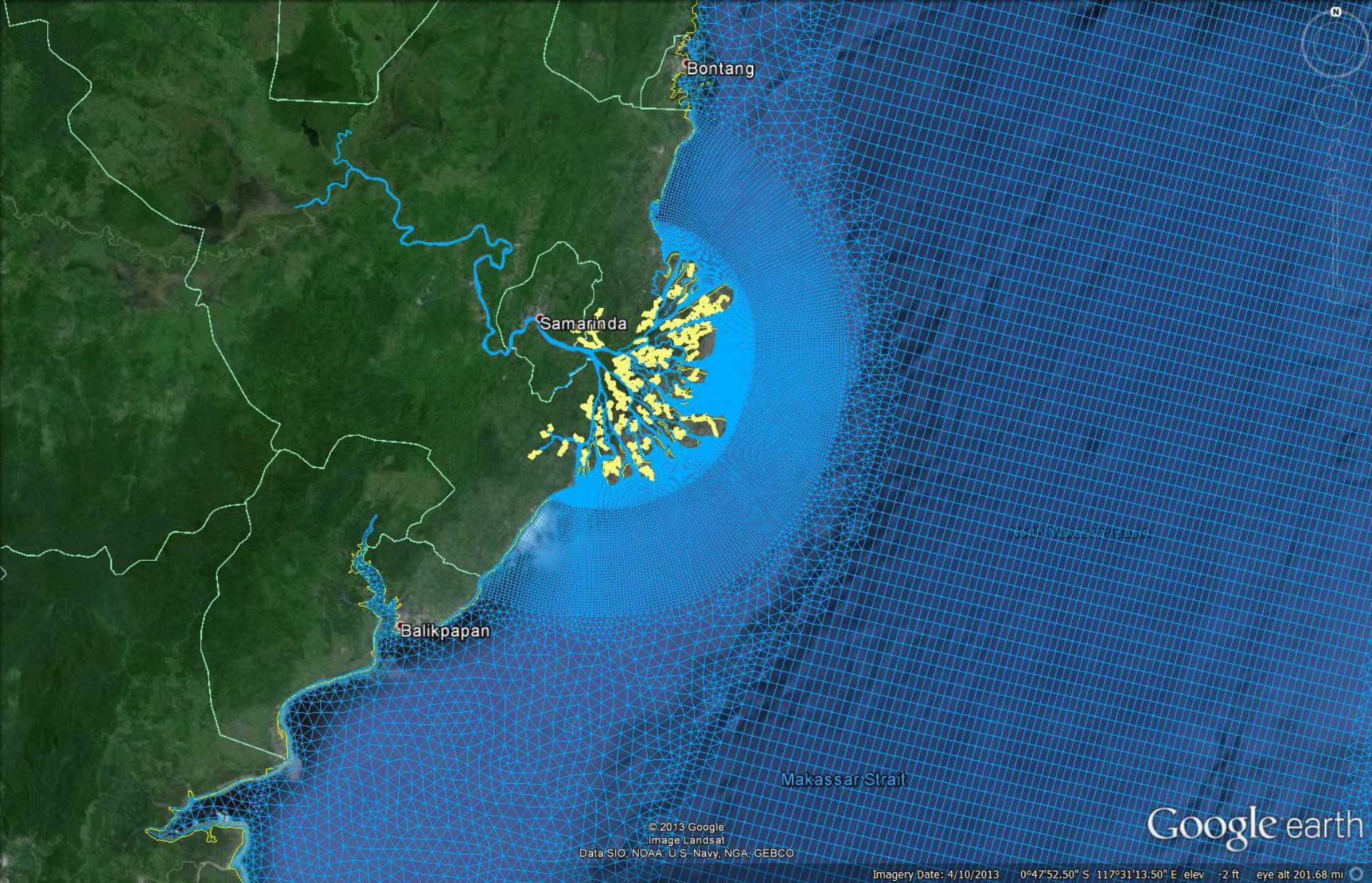


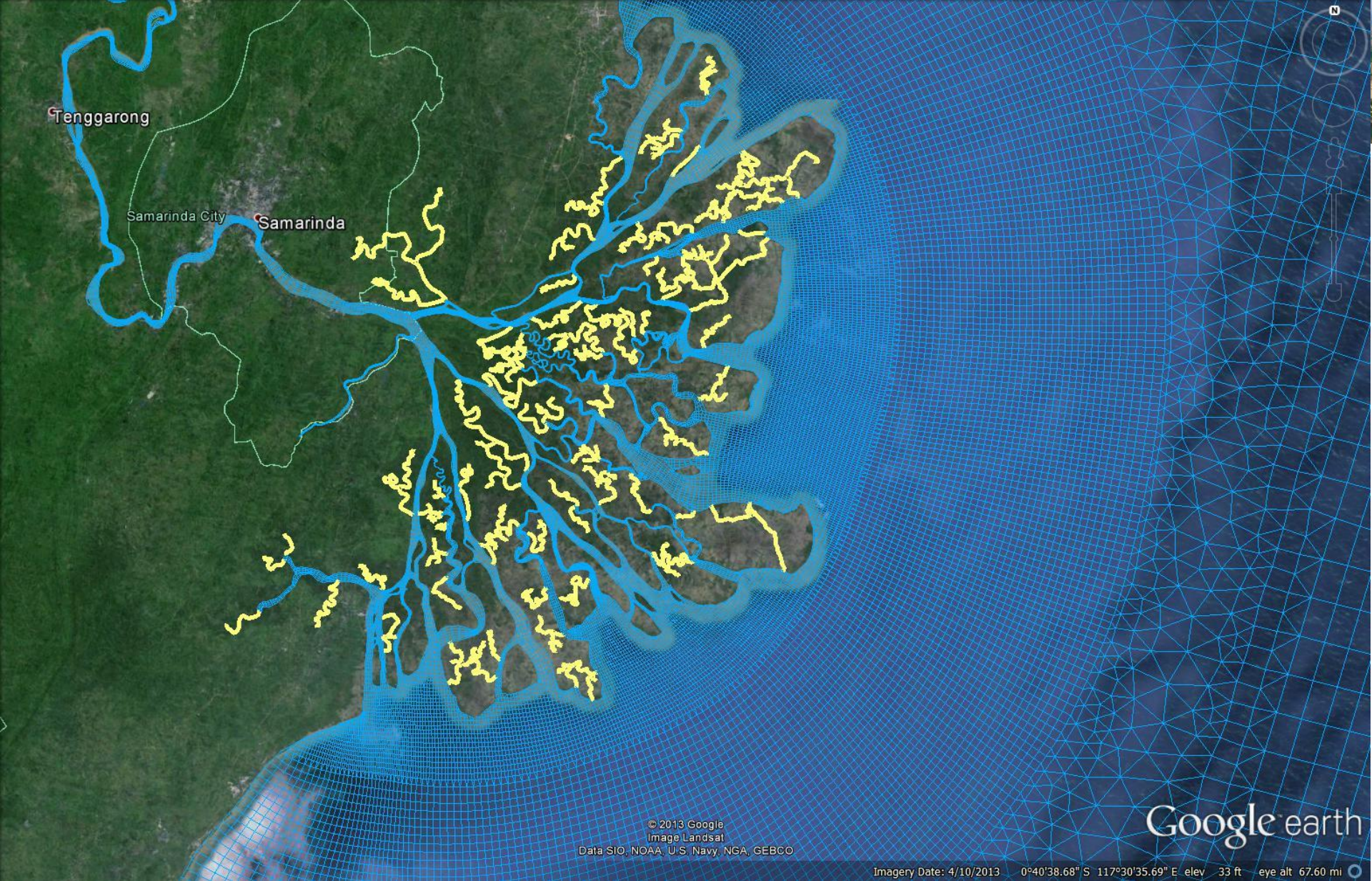
US Dept of State Geographer
Image Landsat
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Data SIO, NOAA, U.S. Navy, NGA, GEBCO

Google earth

Search
Imagery Date: 4/10/2013 1°08'23.28" S 119°55'37.54" E elev -593 ft eye alt 4186.37 mi







Tenggarong

Samarinda City

Samarinda

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Image Landsat
Data SIO, NOAA, U.S. Navy, NGA, GEBCO

Google earth

Imagery Date: 4/10/2013 0°40'38.68" S 117°30'35.69" E elev 33 ft eye alt 67.60 mi

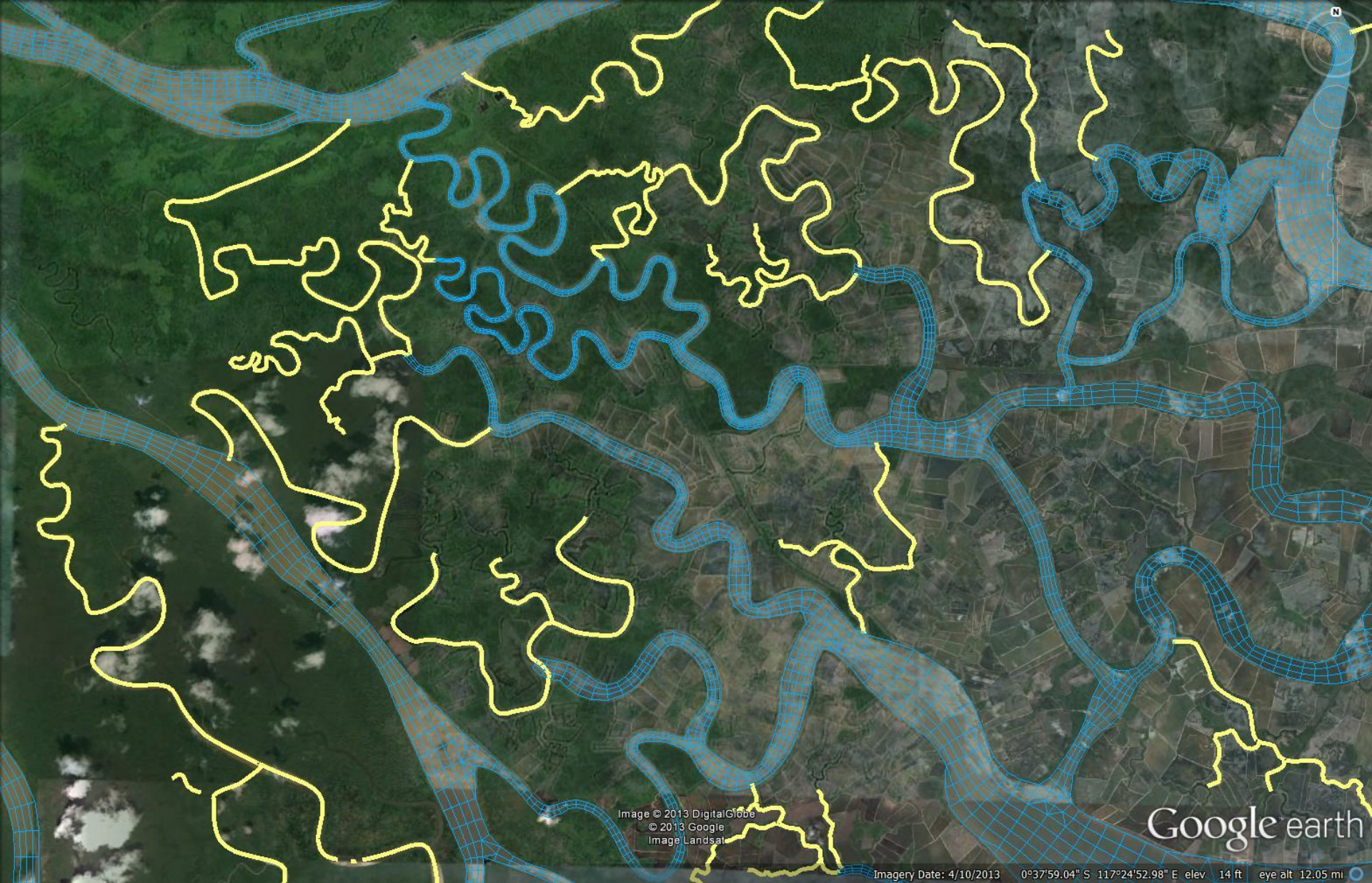
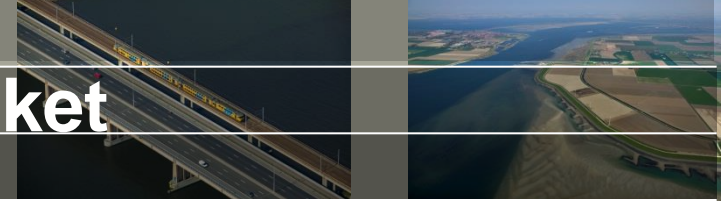


Image © 2013 DigitalGlobe
© 2013 Google
Image Landsat

Google earth

Imagery Date: 4/10/2013 0°37'59.04" S 117°24'52.98" E elev 14 ft eye alt 12.05 mi

Free surface flows: a niche market

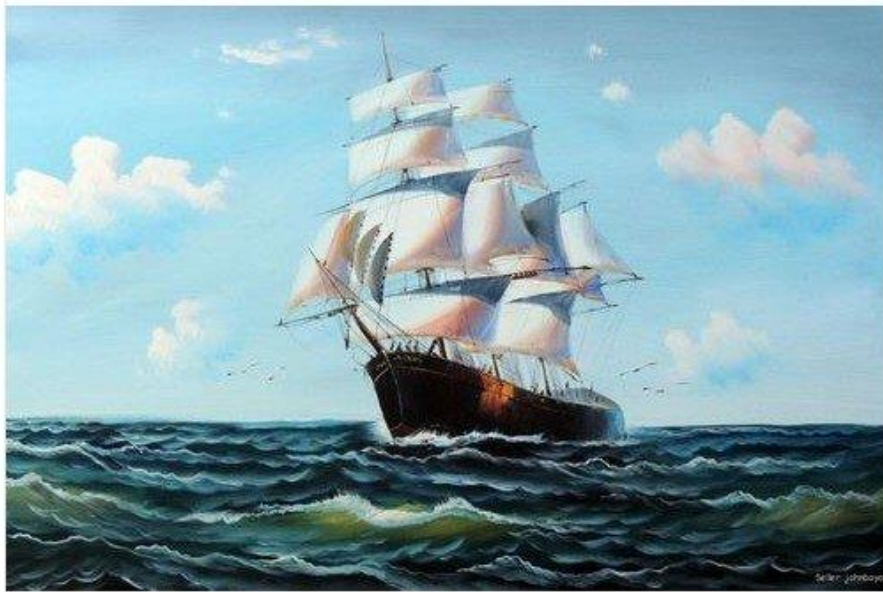


Mostly based upon hydrostatic pressure assumption

Horizontal scale \gg Vertical scale

Wave propagation speed may be large

Flow speed and Wave speed, depth 5 km



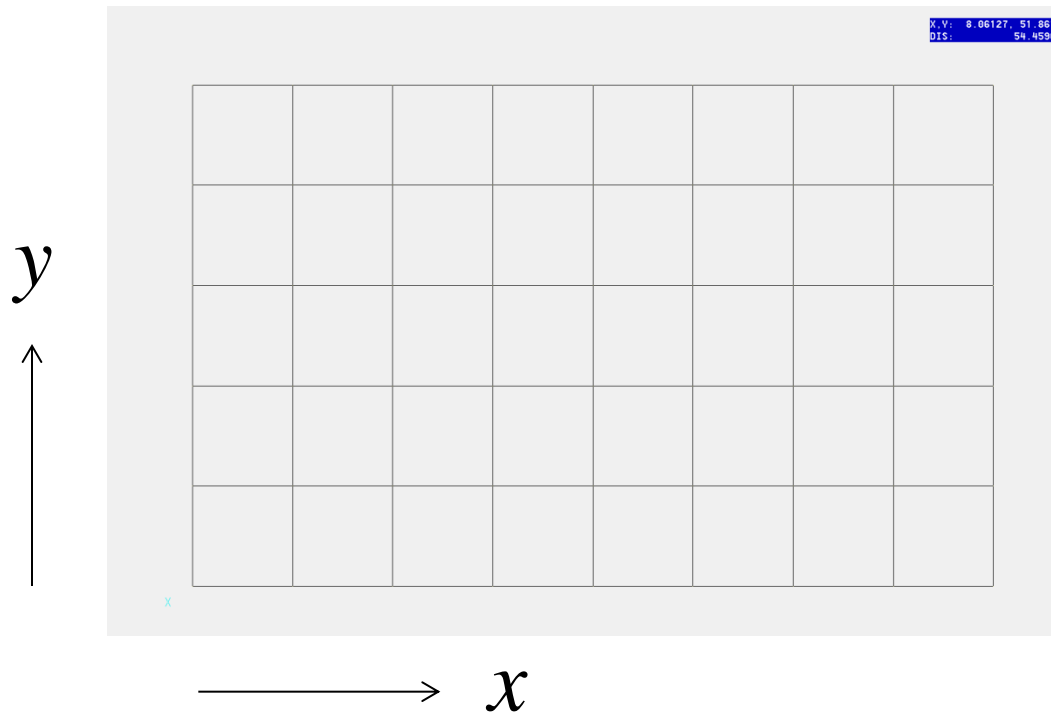
0-2 m/s => Advection maybe explicit



221 m/s => Pressures allways implicit

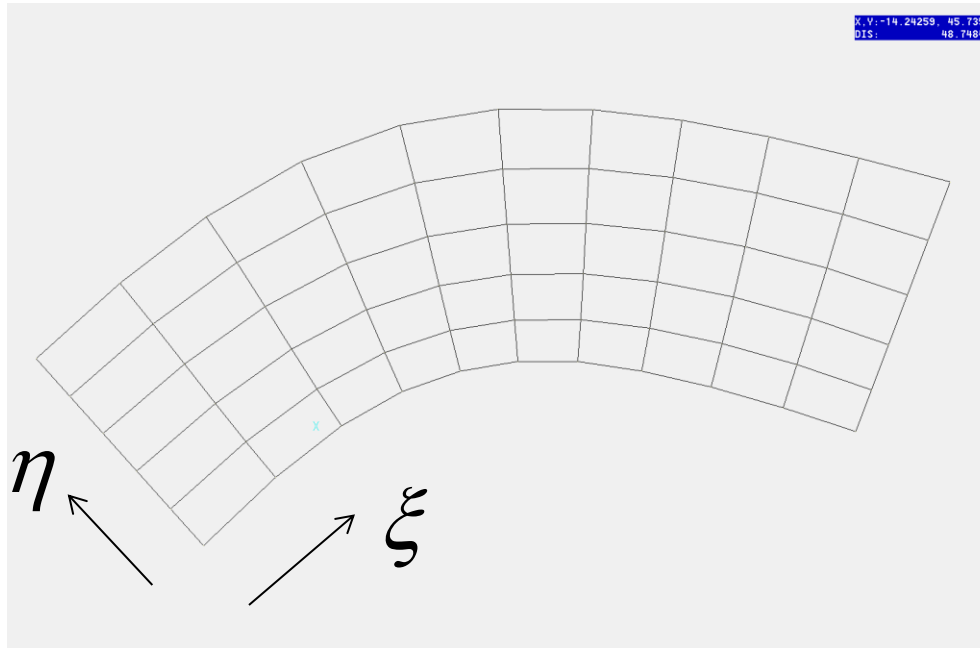
Advection & pressure rectilinear coordinates

$$\frac{\partial U}{\partial t} + U \frac{\partial U}{\partial x} + V \frac{\partial U}{\partial y} + g \frac{\partial \zeta}{\partial x} \dots =$$



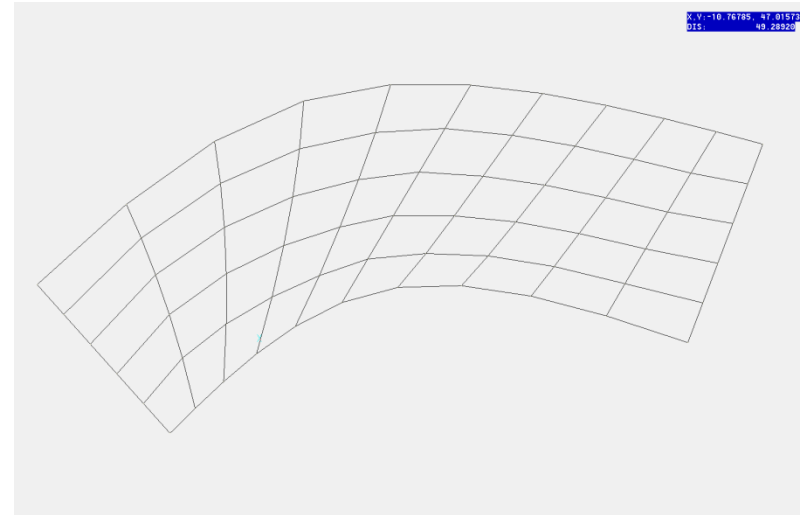
Momentum equation orthogonal curvilinear coor.

$$\frac{\partial U}{\partial t} + \frac{U}{\sqrt{G_{\xi\xi}}} \frac{\partial U}{\partial \xi} + \frac{V}{\sqrt{G_{\eta\eta}}} \frac{\partial U}{\partial \eta} + \frac{UV}{\sqrt{G_{\xi\xi}}\sqrt{G_{\eta\eta}}} \frac{\partial \sqrt{G_{\xi\xi}}}{\partial \eta} - \frac{VW}{\sqrt{G_{\xi\xi}}\sqrt{G_{\eta\eta}}} \frac{\partial \sqrt{G_{\eta\eta}}}{\partial \xi} + \frac{g}{\sqrt{G_{\xi\xi}}} \frac{\partial \zeta}{\partial \xi} \dots =$$



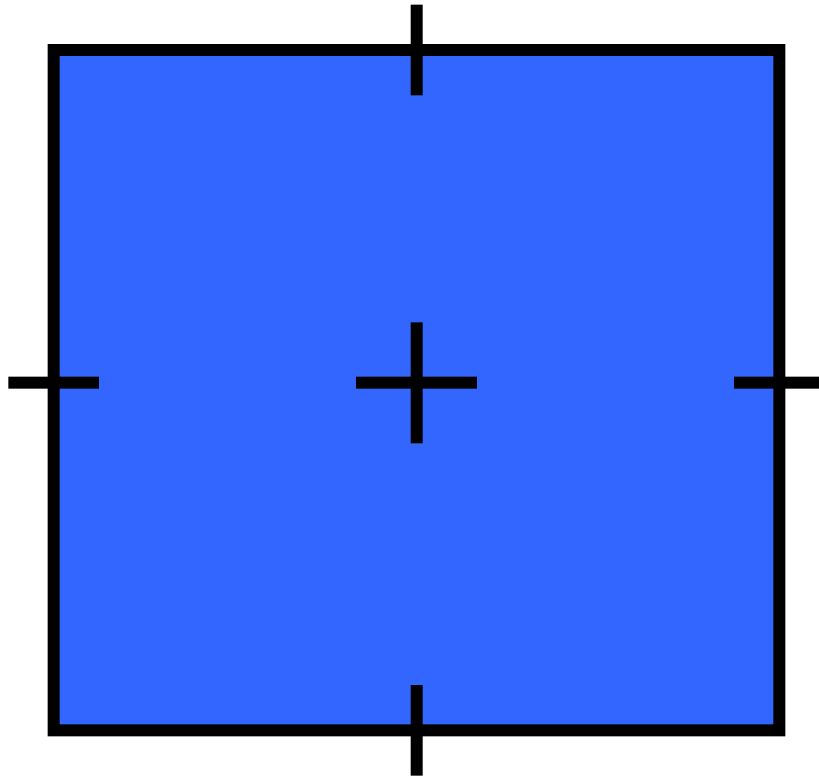
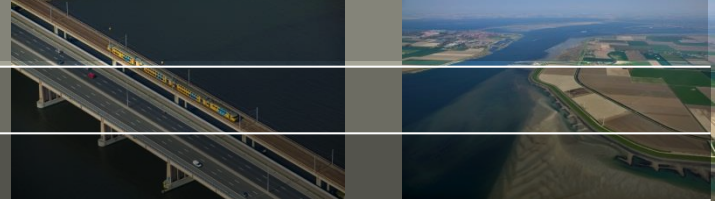
Momentum equation non orthogonal coordinates

$$\begin{aligned}
 & \frac{\partial U}{\partial t} + V^2 \left(\frac{\sqrt{G_{\eta\eta}}}{J} \right)_{\xi} + \left(\frac{\sqrt{G_{\xi\xi}}}{\sqrt{G_{\eta\eta}}} \right) UV \left(\frac{\sqrt{G_{\xi\xi}}}{J} \right)_{\eta} \\
 & + \frac{1}{J^2} \left(+\sqrt{G_{\eta\eta}} y_{\eta} U \frac{\partial [x_{\xi} U]}{\partial \xi} + \sqrt{G_{\xi\xi}} y_{\eta} V \frac{\partial [x_{\xi} U]}{\partial \eta} \right) \\
 & + \frac{1}{J^2} \left(+\sqrt{G_{\xi\xi}} y_{\eta} U \frac{\partial [x_{\eta} V]}{\partial \xi} + \frac{G_{\xi\xi}}{\sqrt{G_{\eta\eta}}} y_{\eta} V \frac{\partial [x_{\eta} V]}{\partial \eta} \right) \\
 & + \frac{1}{J^2} \left(-\sqrt{G_{\eta\eta}} x_{\eta} U \frac{\partial [y_{\xi} U]}{\partial \xi} - \sqrt{G_{\xi\xi}} x_{\eta} V \frac{\partial [y_{\xi} U]}{\partial \eta} \right) \\
 & + \frac{1}{J^2} \left(-\sqrt{G_{\xi\xi}} x_{\eta} U \frac{\partial [y_{\eta} V]}{\partial \xi} - \frac{G_{\xi\xi}}{\sqrt{G_{\eta\eta}}} x_{\eta} V \frac{\partial [y_{\eta} V]}{\partial \eta} \right) + \dots = \\
 & + \frac{g}{J} \left(\sqrt{G_{\eta\eta}} \frac{\partial \zeta}{\partial \xi} - \frac{(x_{\xi} x_{\eta} + y_{\xi} y_{\eta})}{\sqrt{G_{\eta\eta}}} \frac{\partial \zeta}{\partial \eta} \right)
 \end{aligned}$$



$$J = x_{\xi} y_{\eta} - y_{\xi} x_{\eta}$$

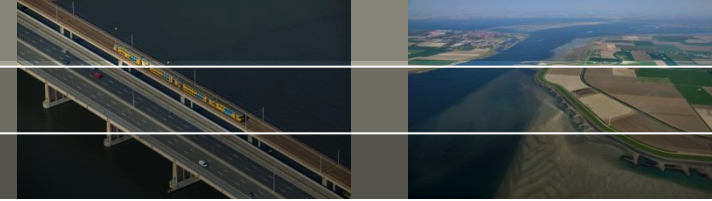
Staggered approach



Pressures / concentrations in cell centres

Velocities at cell faces

Finite volume approach



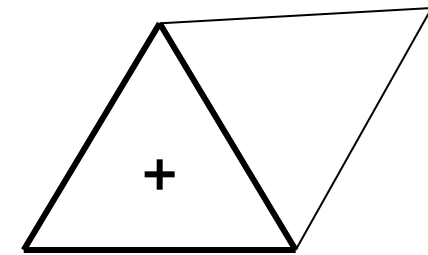
Conservation of:

$$\frac{\partial V}{\partial t} = \sum_{in\zeta} Q - \sum_{out\zeta} Q$$

Volume

$$\frac{\partial Vc}{\partial t} = \sum_{in\zeta} Qc_{in} - \sum_{out\zeta} Qc_{out}$$

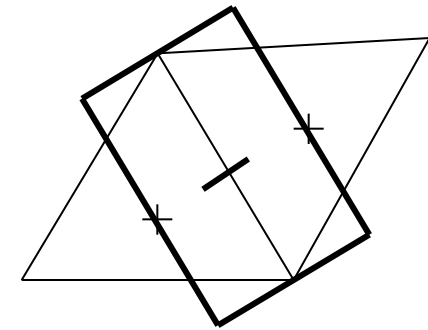
Mass



Cell center

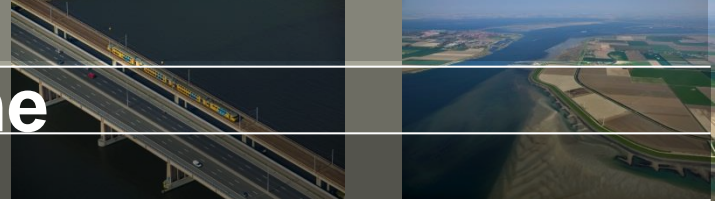
$$\frac{\partial V_u \rho u}{\partial t} = \sum_{inu} Q \rho_{in} u_{in} - \sum_{outu} Q \rho_{out} u_{out} + \sum F_u$$

Momentum



Cell face

Time integration 2D, theta scheme



$$\frac{u^{n+1} - u^n}{\Delta t} + \frac{g}{\Delta x} \left\{ \theta (\zeta_2^{n+1} - \zeta_1^{n+1}) + (1 - \theta) (\zeta_2^n - \zeta_1^n) \right\} + bu^{n+1} = d$$

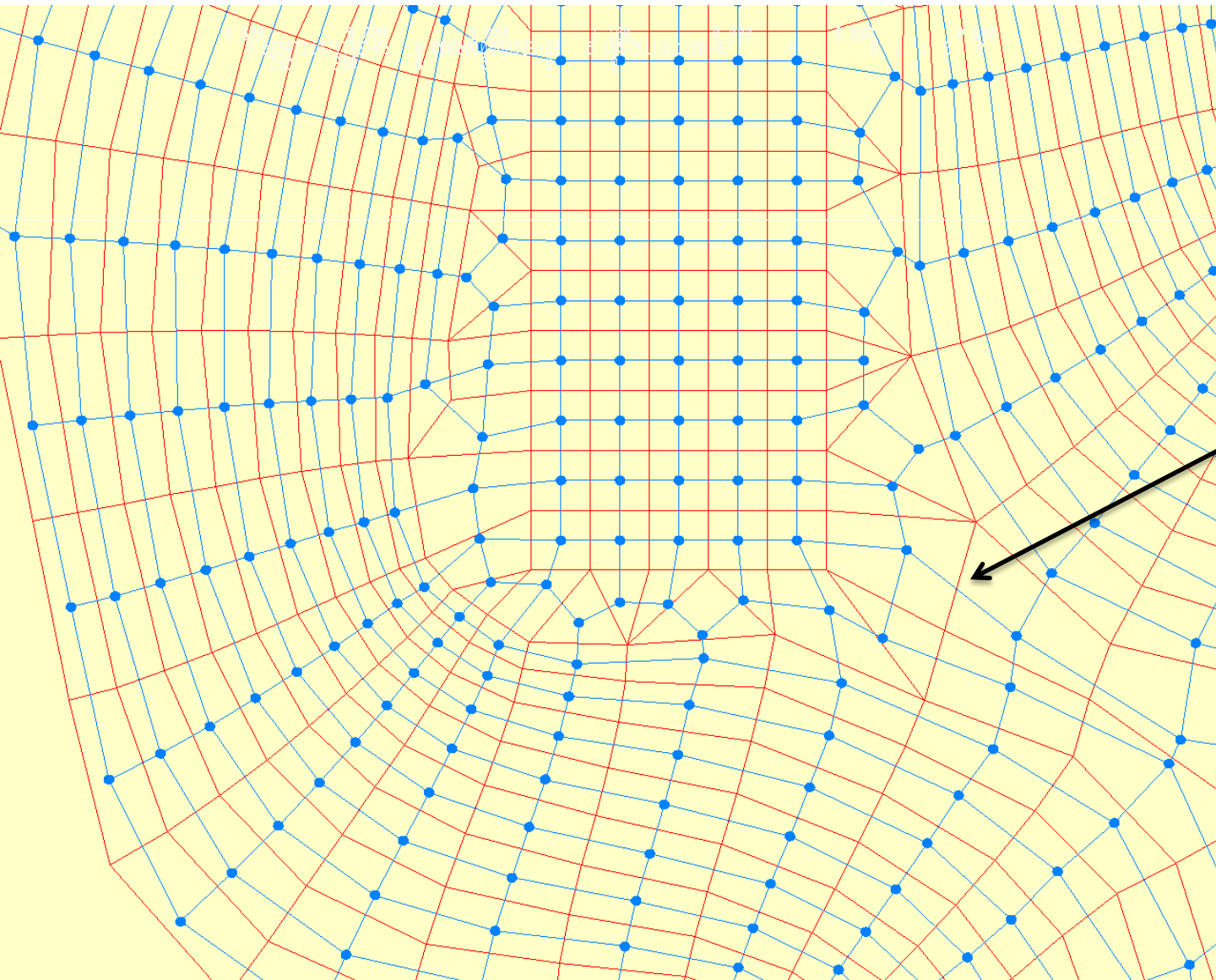
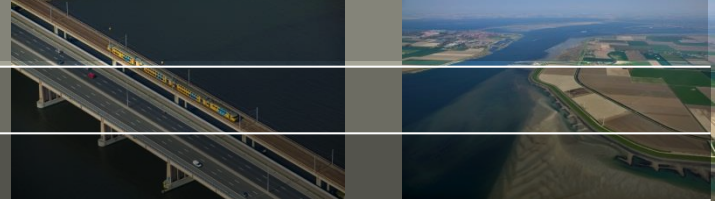
Acceleration + pressure + bedfriction = -advection

Rewrite as: $u^{n+1} = R_u + F_u (\zeta_2^{n+1} - \zeta_1^{n+1})$

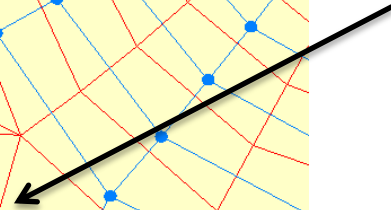
Substitute in: $A_\zeta \frac{\zeta_2^{n+1} - \zeta_1^{n+1}}{\Delta t} + \theta (A_{u2} u_2^{n+1} - A_{u1} u_1^{n+1}) + (1 - \theta) (A_{u2} u_2^n - A_{u1} u_1^n) = Q_\zeta$

Solve sparse pressure matrix.

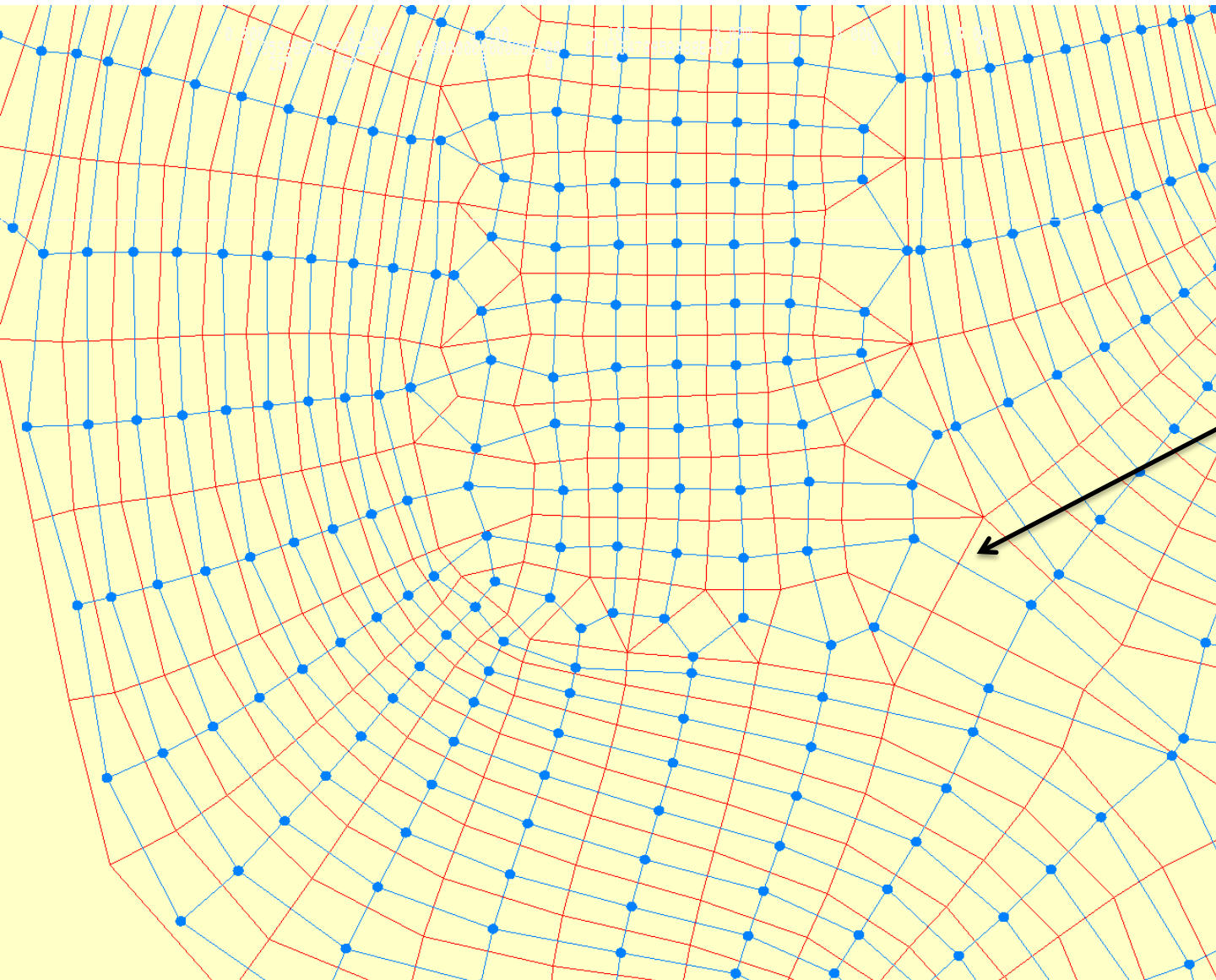
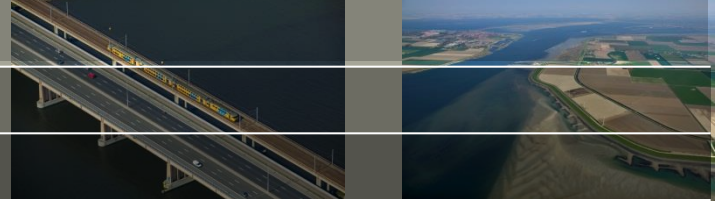
Not Orthogonal



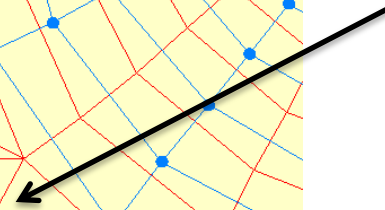
Non orthogonal



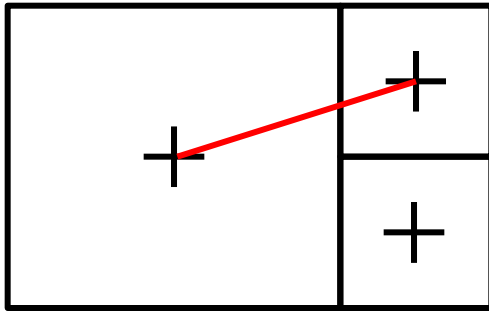
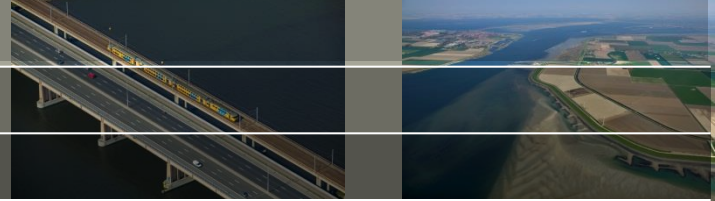
Orthogonal !



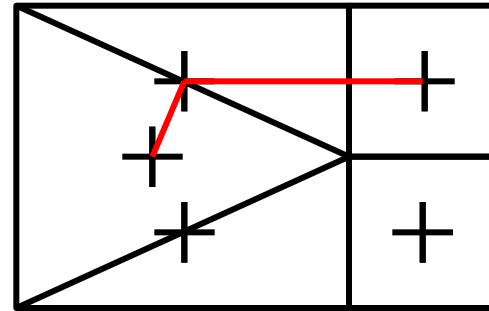
Orthogonal



Orthogonal grid refinement



Non orthogonal

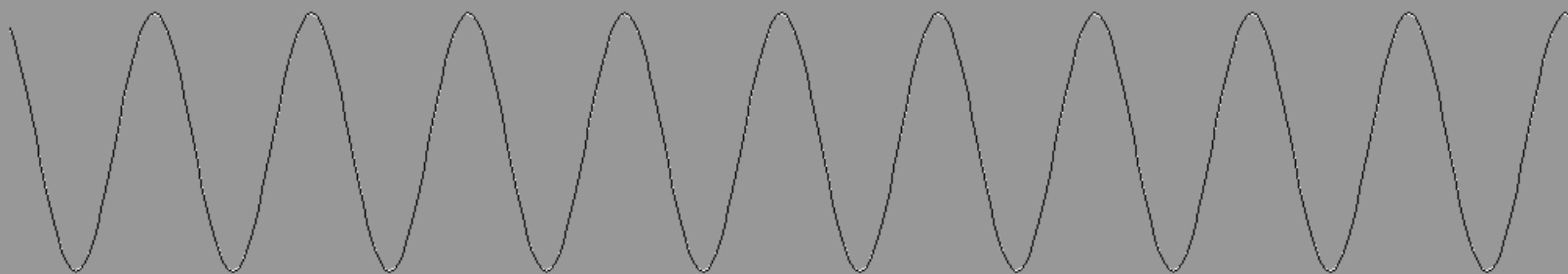


Orthogonal


```

19920831_002000 dt: 600.000 Avg.dt:600.000 CPU/step: 0.000 Tot: 0.0 Sol/Rest:.00E+00 Saver: 0.00000000E+00 Samtot:0.00000000E+0
k/nplot: 1 180 znod(nn): 0.14679779E+00 Uoll: 0.22302255E+17 Uler: 0.80000000E+01 #setb: 0 #dt: 2 #itsol: 0
#ndx: 360 #lnx: 360 #kmx: 0 #CG: 0 #Gauss: 360 #slit: 0 iad: 0 5 runid: equatorid

```



Test teta scheme: Free damped linear wave: teta = 0.55, ndt = 72

-0.300+
-0.718

|
395.6

Forced amplitude = 0.000000 (m), ndx = 36 , ndt = 72, of1 = 0.500019

Free amplitude = 0.149214 (m), ndx = 36 , ndt = 30, of1 = 1.193663

Total amplitude = 0.149214 (m)

Computed amplitude = 0.148455 (m), comp/analytic= 0.995

Teta = 0.55000 , Manlin = 4.00000 , Umod = 0.00477

Nforced = 0.03 , Nfree = 0.07 , Dept = 5000.00

Water level
(m)



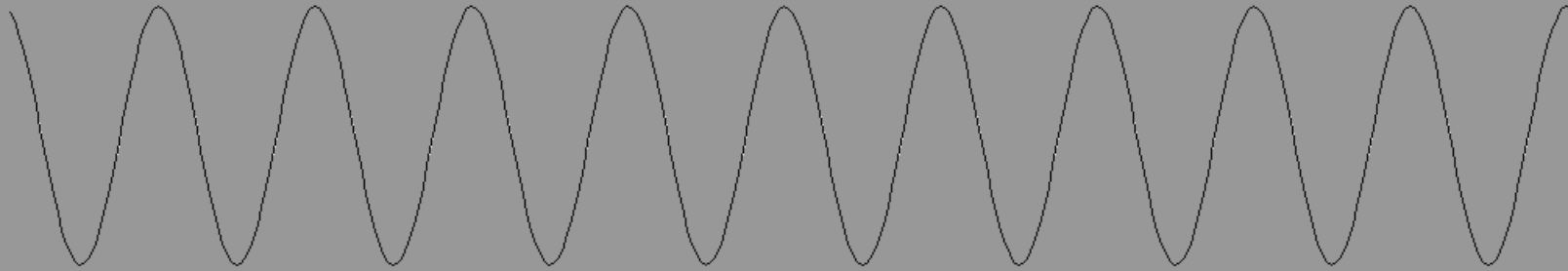
x



```

19920831_001000 dt: 300.000 Avg.dt:300.000 CPU/step: 0.000 Tot: 0.0 Sol/Rest:.00E+00 Saver: 0.00000000E+00 Samtot:0.00000000E+00
k/nplot: 1 180 znod(nn): 0.14935910E+00 Vol1: 0.22302255E+17 U1er: -.12000000E+02 #setb: 0 #dt: 2 #itsol: 0
#ndx: 360 #lnx: 360 #kmx: 0 #CG: 0 #Gauss: 360 #slit: 0 iad: 0 5 runid: equator1d

```



Test teta scheme: Free damped linear wave: teta = 0.501, ndt = 144

-0.300+
-0.718

|
395.6

Forced amplitude = 0.000000 (m), ndx = 36 , ndt = 144, cf1 = 0.250010

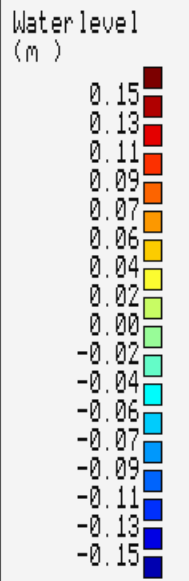
Free amplitude = 0.149606 (m), ndx = 36 , ndt = 60, cf1 = 0.596831

Total amplitude = 0.149606 (m)

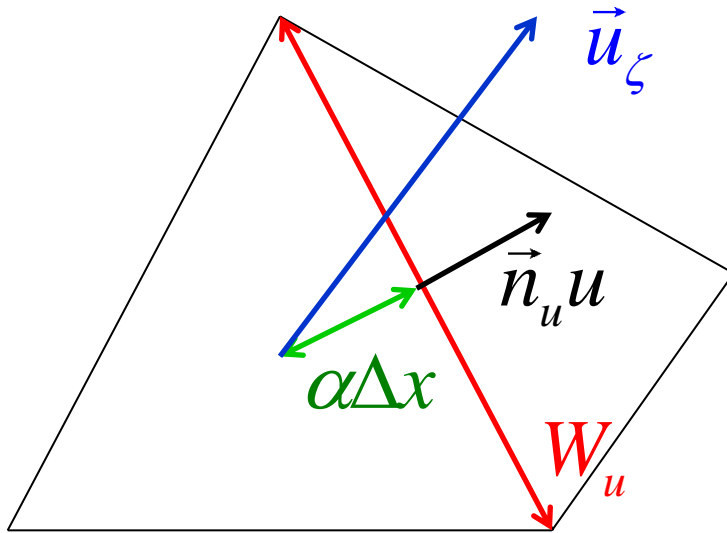
Computed amplitude = 0.149359 (m), comp/analytic= 0.998

Teta = 0.50100 , Manlin = 4.00000 , Umod = 0.00477

Nforced = 0.01 , Nfree = 0.03 , Dept = 5000.00



Faces to center and centers to face



$$\vec{u}_\zeta = \frac{1}{A_\zeta} \sum^{faces} \alpha\Delta x W_u \vec{n}_u u$$

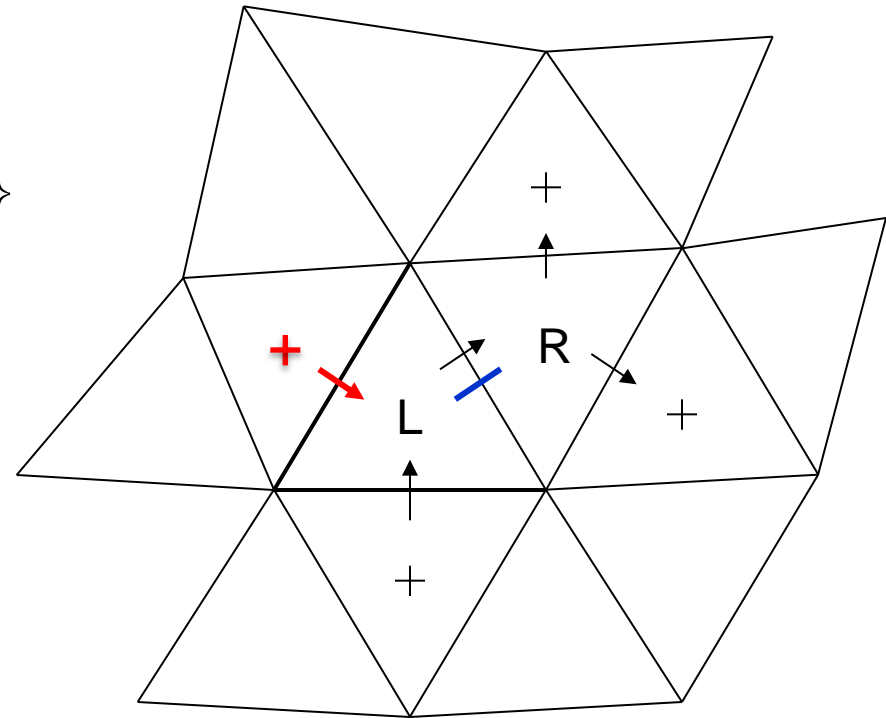
$$V_u = \alpha V_L + (1 - \alpha) V_R$$

Momentum advection ~ Kramer Stelling

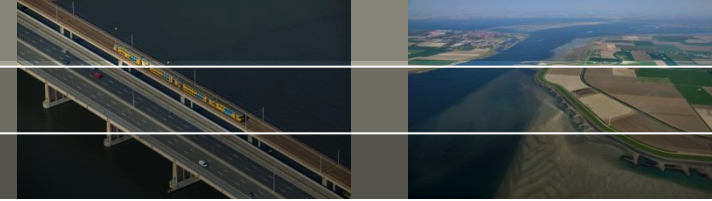
Advection term gets contributions assembled at Left and Right nodes

$$\frac{1}{V_u} \left\{ \begin{array}{l} \alpha \left(\sum_{inL} Q(u_{in} - u) - \sum_{outL} Q(u_{out} - u) \right) + \\ (1 - \alpha) \left(\sum_{inR} Q(u_{in} - u) - \sum_{outR} Q(u_{out} - u) \right) \end{array} \right\}$$

$$V_u = \alpha V_L + (1 - \alpha) V_R$$



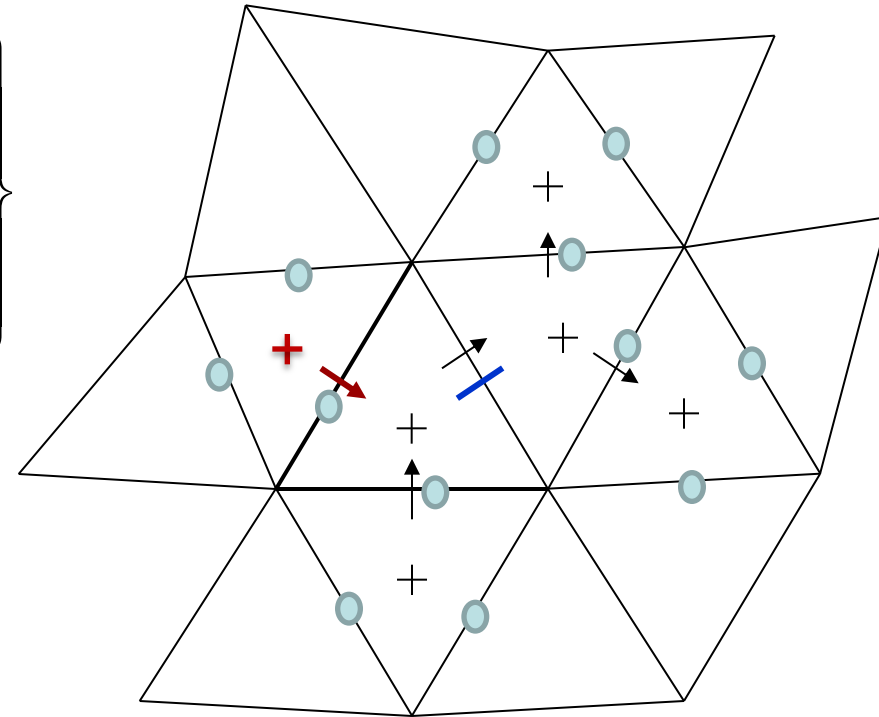
Momentum advection



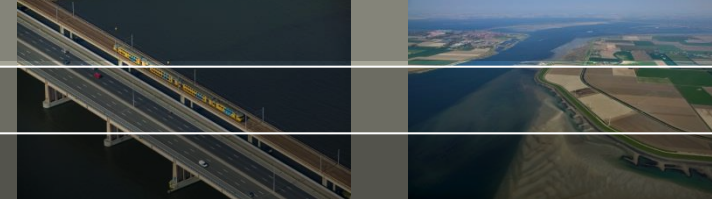
Velocity points involved in first order

$$\frac{1}{V_u} \left\{ \begin{array}{l} \alpha \left(\sum_{inL} Q(u_{in} - u) - \sum_{outL} Q(u_{out} - u) \right) + \\ (1 - \alpha) \left(\sum_{inR} Q(u_{in} - u) - \sum_{outR} Q(u_{out} - u) \right) \end{array} \right\}$$

$$V_u = \alpha V_L + (1 - \alpha) V_R$$



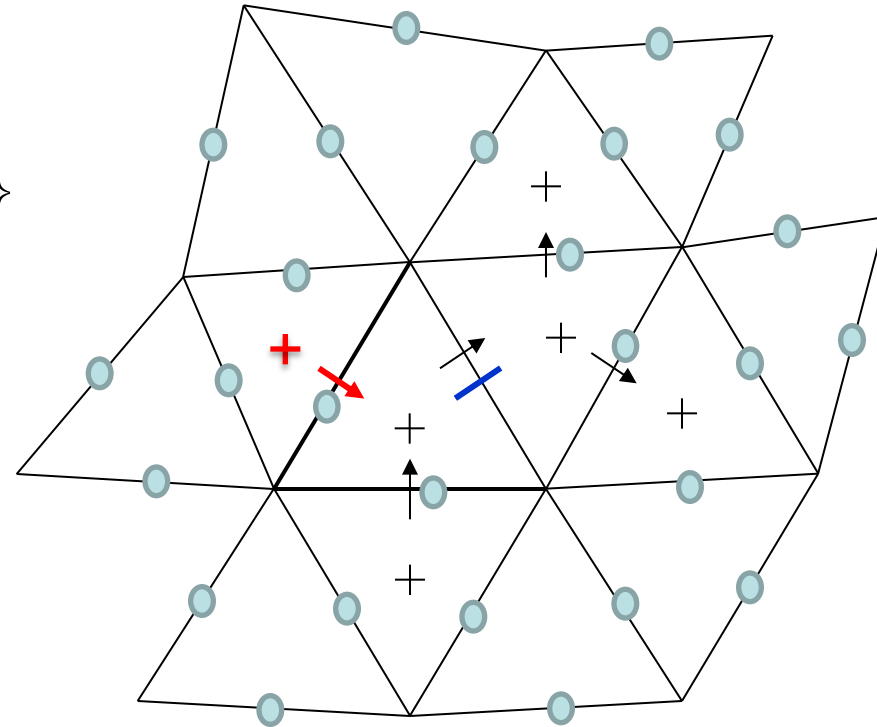
Momentum advection



Velocity points involved in limited higher order

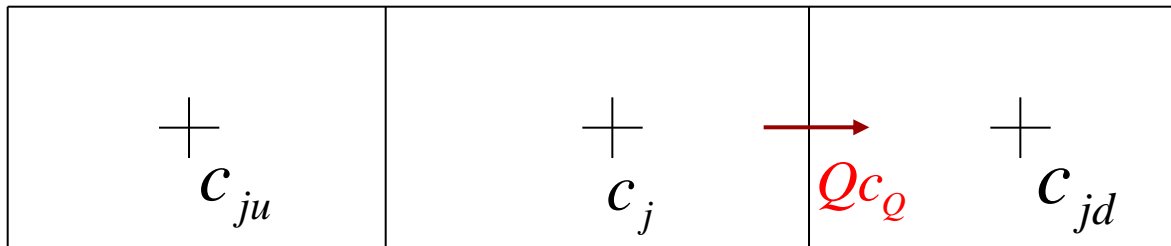
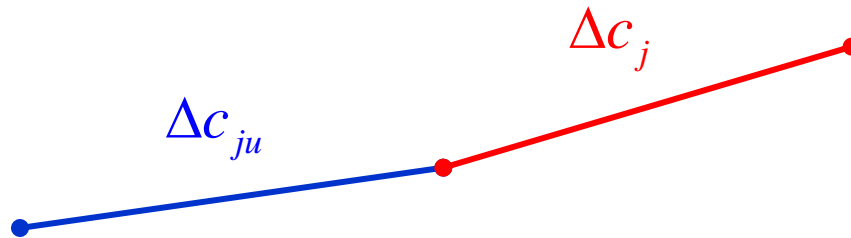
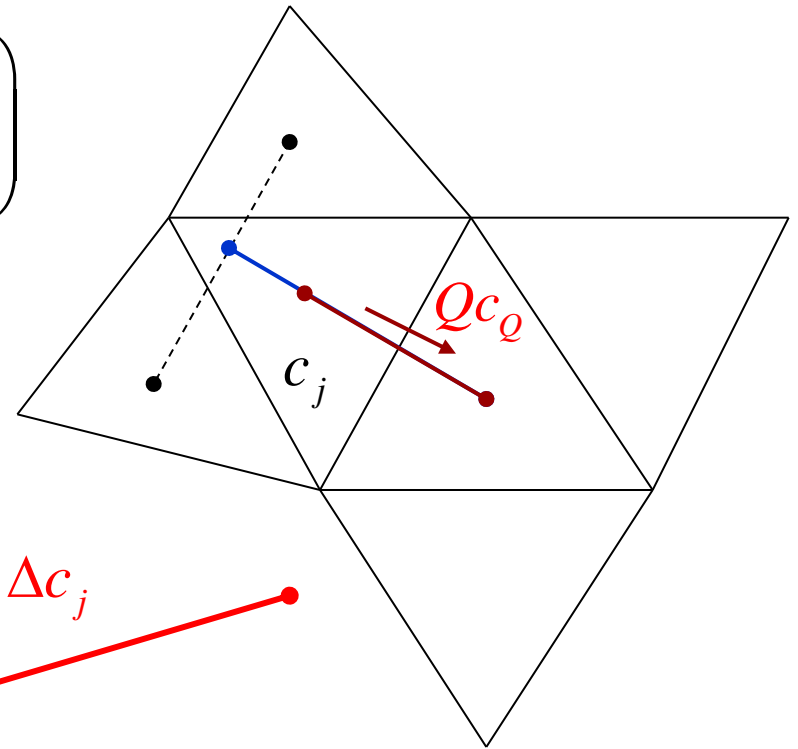
$$\frac{1}{V_u} \left\{ \begin{array}{l} \alpha \left(\sum_{inL} Q(u_{in} - u) - \sum_{outL} Q(u_{out} - u) \right) + \\ (1 - \alpha) \left(\sum_{inR} Q(u_{in} - u) - \sum_{outR} Q(u_{out} - u) \right) \end{array} \right\}$$

$$V_u = \alpha V_L + (1 - \alpha) V_R$$

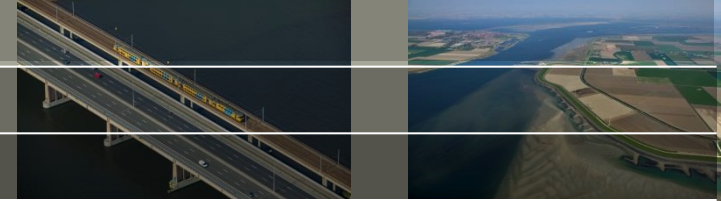


Higher order slope limiter

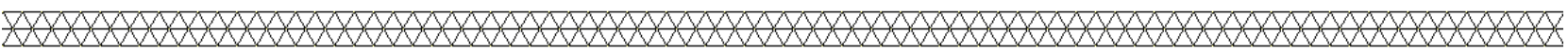
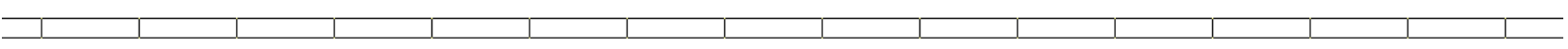
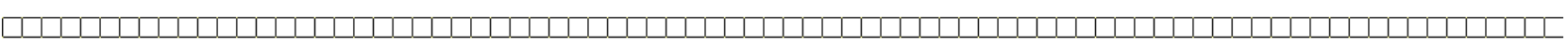
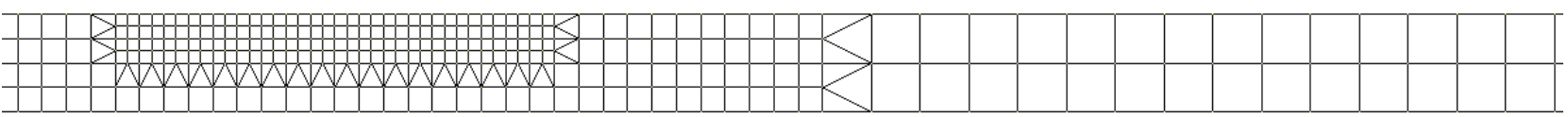
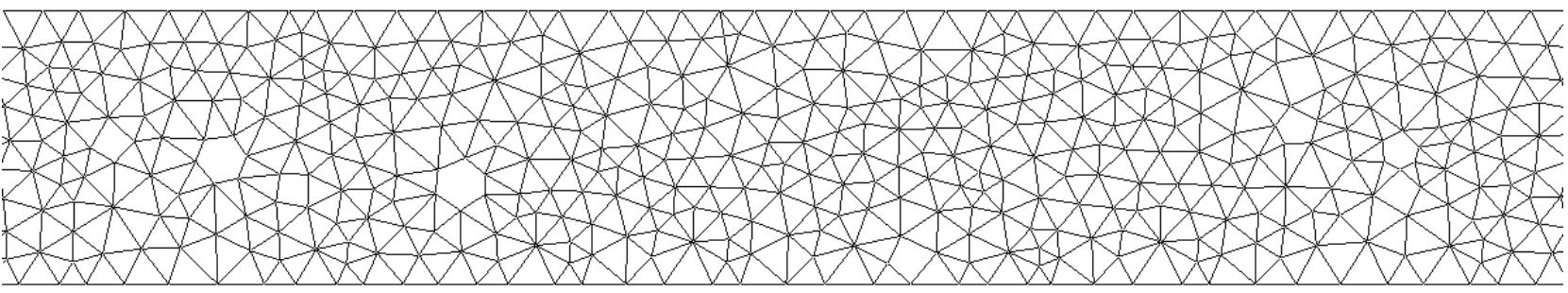
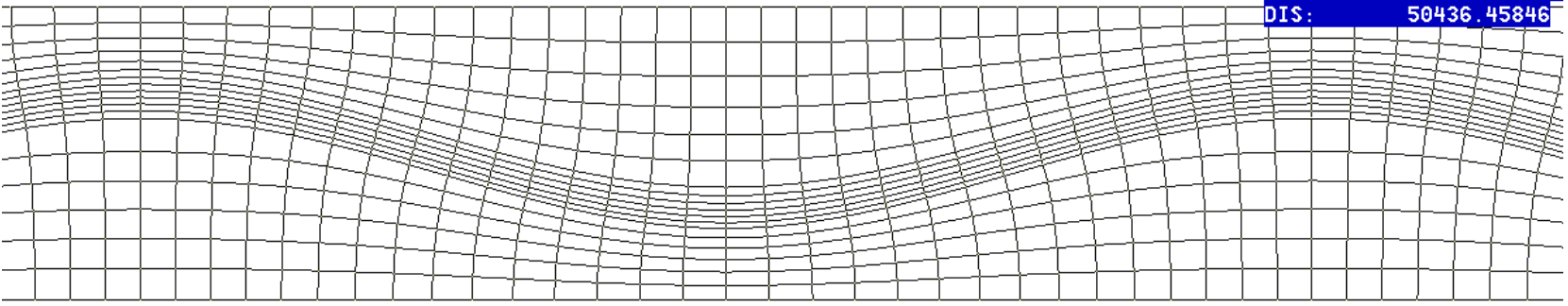
$$c_Q = c_j + \Delta c_j S(\Delta c_{ju}, \Delta c_j) \frac{1}{2} \left(1 - \frac{u_j \Delta t}{\Delta x_j} \right)$$



Dambreak test grids



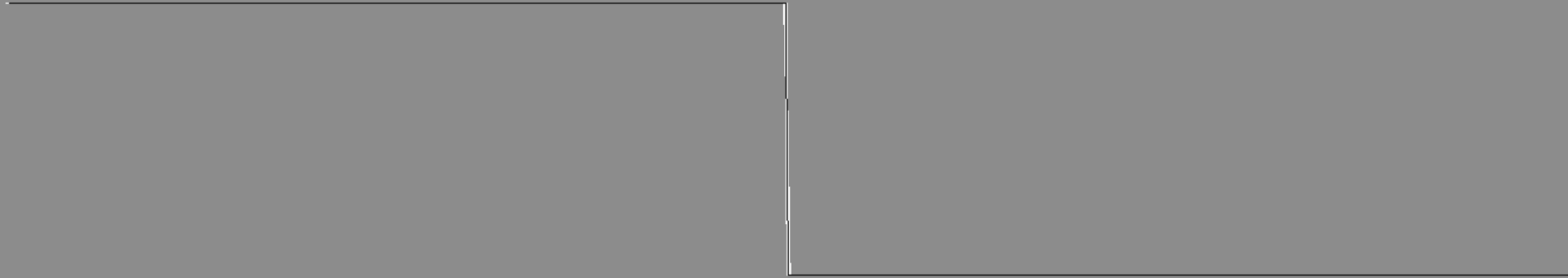
X, Y: 48654.36, 4507.32
DIS: 50436.45846



20061225 000000 dt: 1.000 Avg.dt: 1.000 CPU/step: 0.000 Tot: 0.0 Sol/Rest:.00E+00 Samer: 0.00000000E+00 Samtot:0.0
k/nplot: 1 7849 znod(nn): 0.20000000E+01 Voll: 0.00000000E+00 Vler: 0.00000000E+00 #setb: 0 #dt: 0 #itsol:
#ndx: 15698 #lnx: 24619 #kmx : 0 #CG: 4670 #Gauss: 11028 #slit: 0 iad: 34 5 runid: wetbed

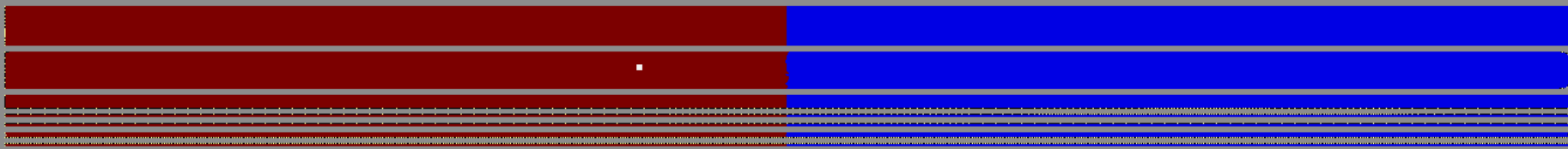
3.010 -

2D



-0.020 +
-0.120E+03

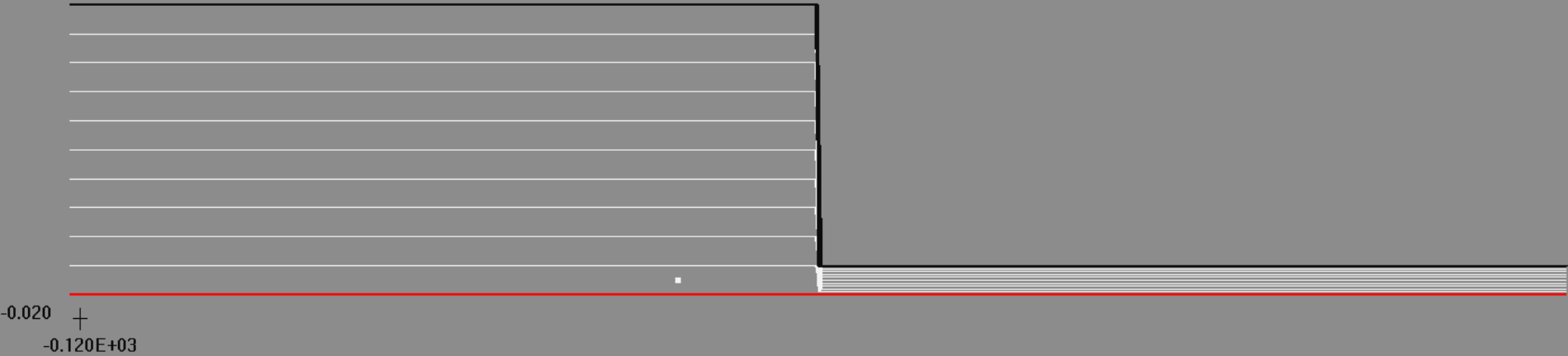
Ave Difference (m) = 0.0004
Rms Difference (m) = 0.0169
Max Difference (m) = 0.9419
Cum Difference (m) = 0.0004



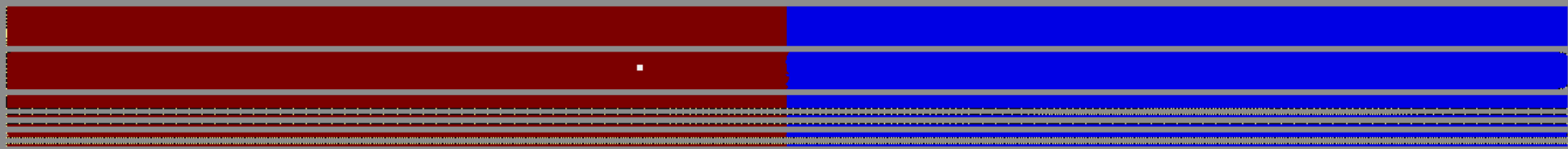
X

3.010 — 20061225 000000 dt: 1.000 Avg.dt: 1.000 CPU/step: 0.000 Tot: 0.0 Sol/Rest:.00E+00 Samer: 0.00000000E+00 Samtot:0.00000000E+00
k/nplot: 1 7849 znod(nn): 0.20000000E+01 Voll: 0.00000000E+00 Vler: 0.00000000E+00 #setb: 0 #dt: 0 #itsol: 0
#ndx: 15698 #lnx: 24619 #kmx : 10 ustB 0.00000 ustW 0.00000 #slit: 0 iad: 34 5 runid: wetbed3d

3D sigma



Ave Difference (m) = 0.0004
Rms Difference (m) = 0.0169
Max Difference (m) = 0.9419
Cum Difference (m) = 0.0004



20061225 000000 dt: 1.000 Avg.dt: 1.000 CPU/step: 0.000 Tot: 0.0 Sol/Rest:.00E+00 Samer: 0.00000000E+00 Samtot:0.00000000E+00
k/nplot: 1 300 znod(nn): 0.20000000E+01 Voll: 0.00000000E+00 Vler: 0.00000000E+00 #setb: 0 #dt: 0 #itsol: 0
#ndx: 600 #lnx: 599 #kmx : 20 ustB 0.00000 ustW 0.00000 #slit: 0 iad: 330 5 runid: wetbedline

3.010 -

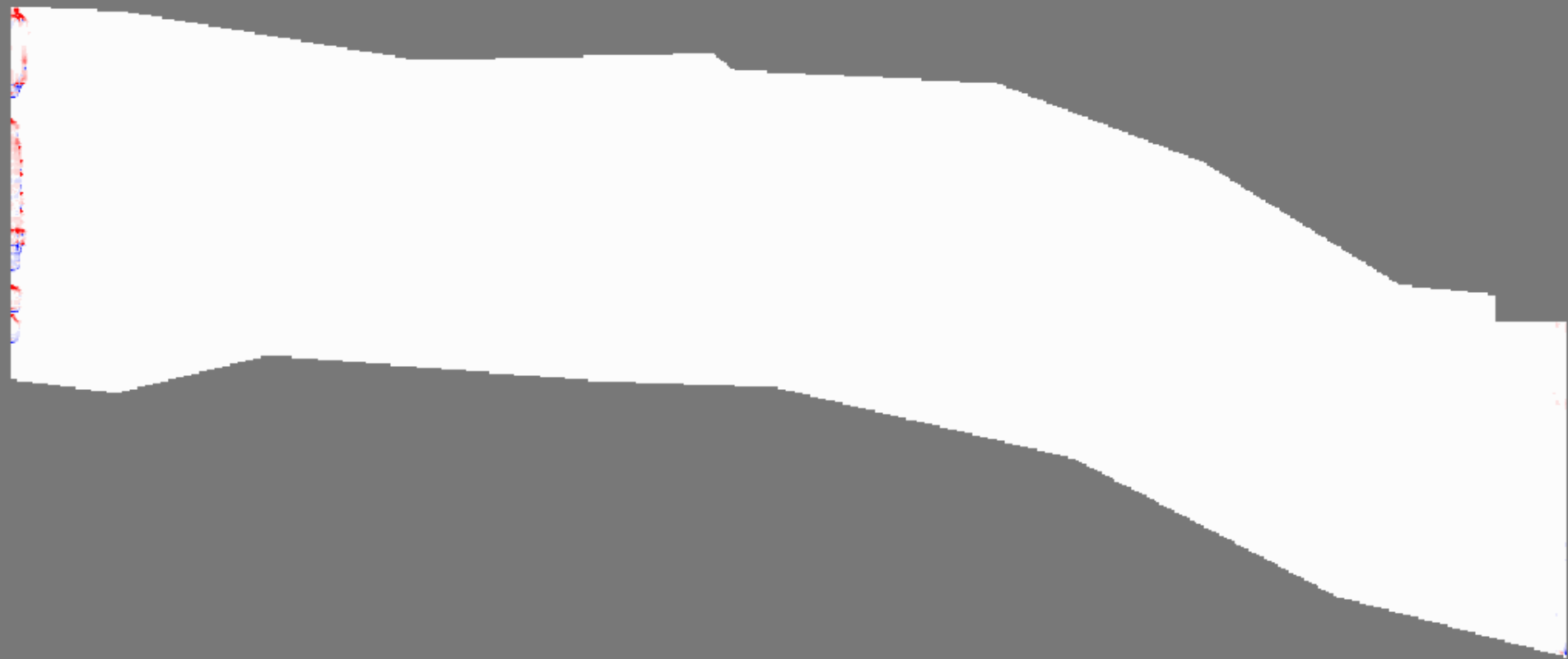
Fixed layers



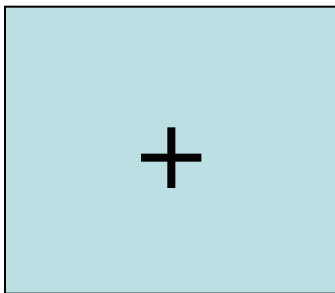
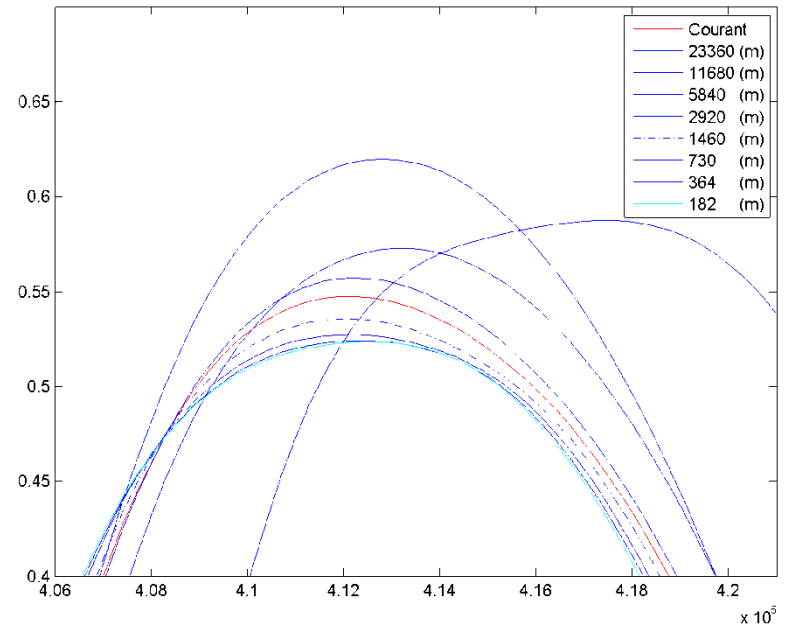
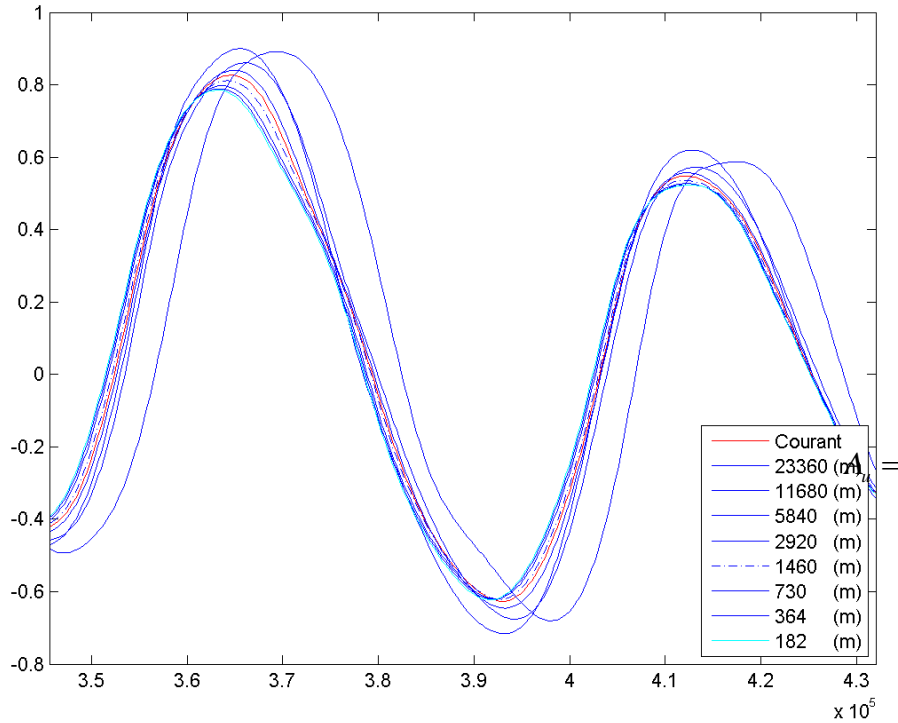
-0.020 +
-0.120E+03

Ave Difference (m) = 0.0000
 Rms Difference (m) = 0.0000
 Max Difference (m) = 0.0000
 Cum Difference (m) = 0.0000

Time S/H/D: 4.000 0.001 0.000 dt: 0.133 Avg.dt: 0.444 CPU/step: 0.047 Tot: 0.3 Sol/Rest: 0.046
k/nplot: 1 100 znod(nn) -999.000000 Uo11: 0.32815816E+06 U1er: -.80945028E-10 #setb: 0 #dt: 8 #itsol: 9
#CG: 9367 #Gauss: 8213 #expl: 0 #wet: 17580 #chkadvd: 789 #nodneg: 0 #slit: 0

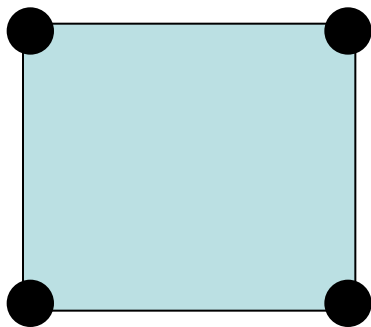
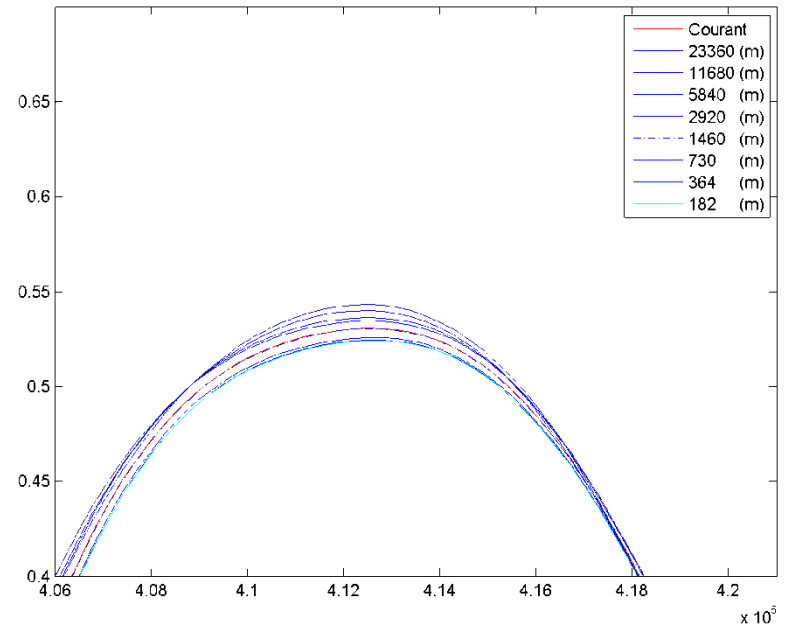
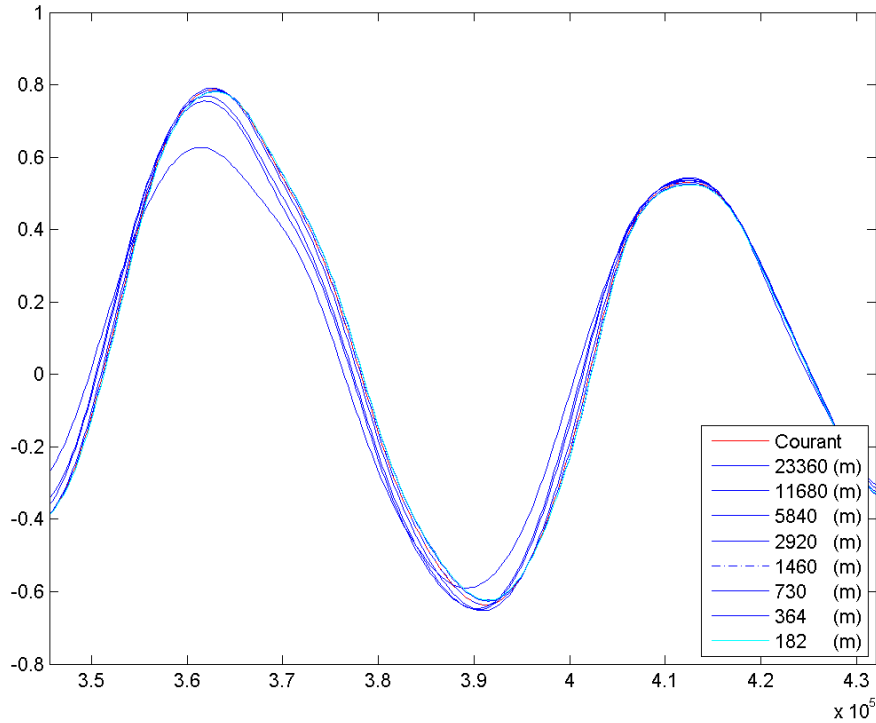


Spatial convergence cell centre bathymetry



Face area \sim maximum level of adjacent centers

Spatial convergence cell corner bathymetry



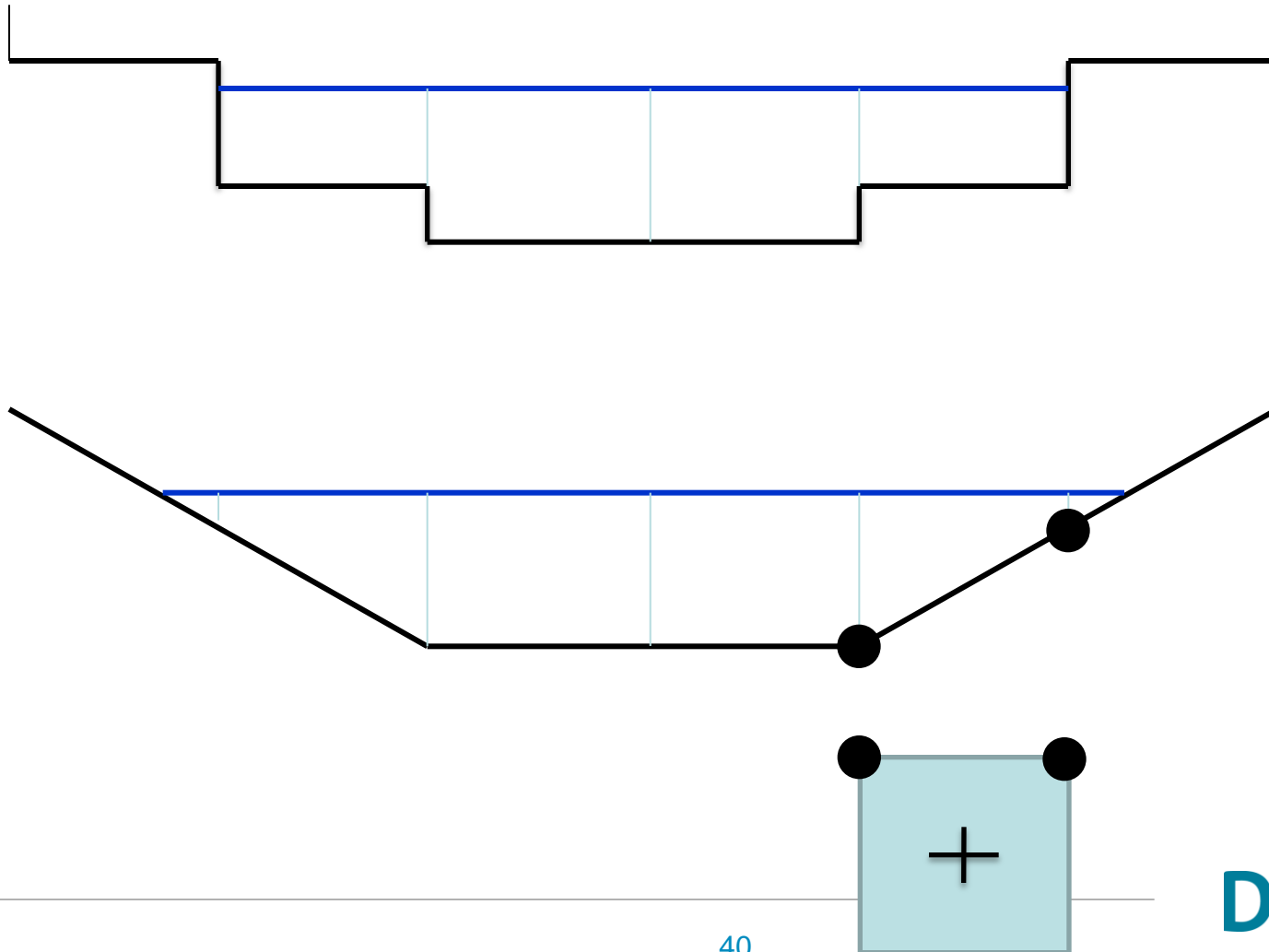
Face area ~ average level of adjacent corners



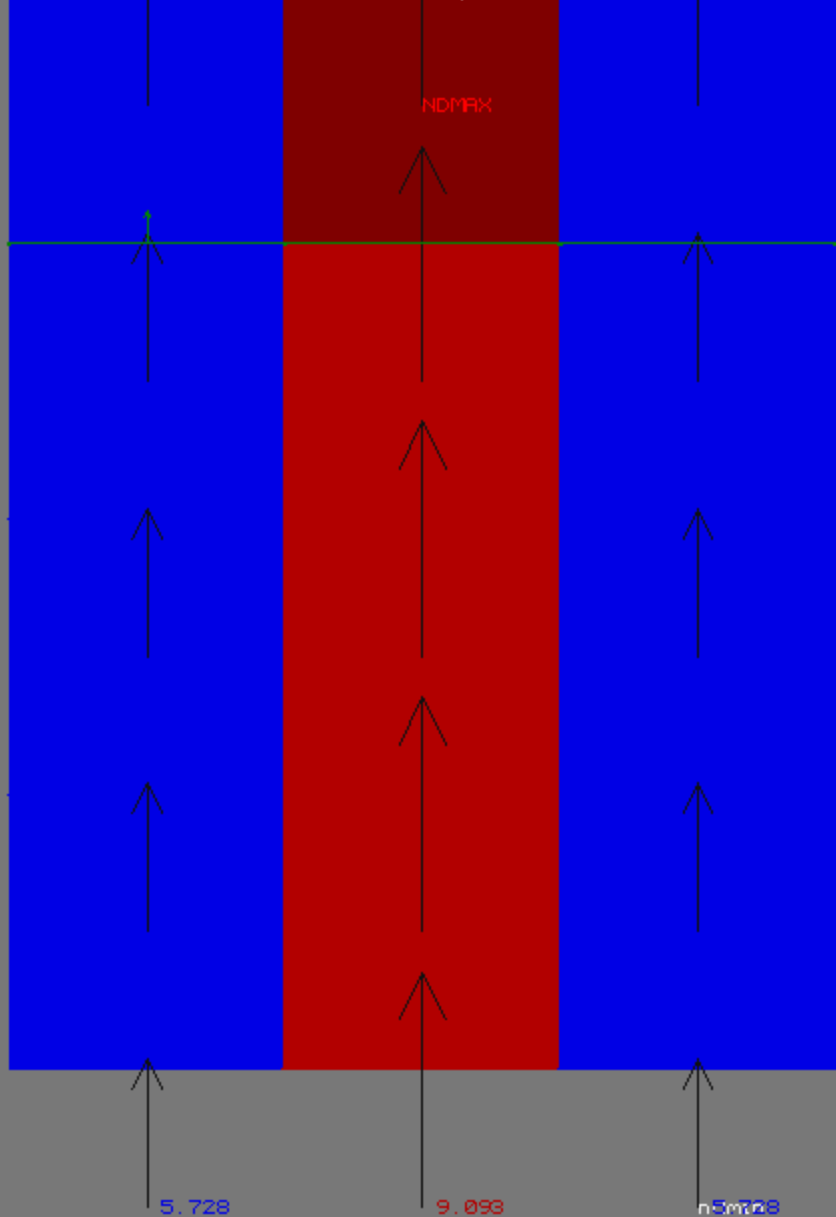
peak flows ~ 6 m/s



Continuous wet area => more gradual drying & flooding

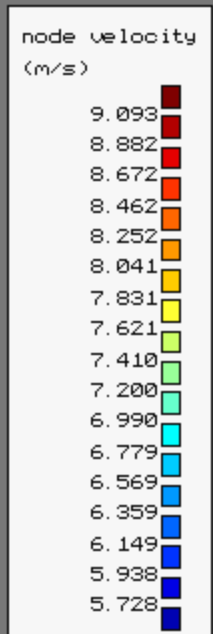


Time S/H/D: 1800.000 0.500 0.021 dt: 0.612 H0g.dt: 0.625 CPU/step: 0.000 Tot: 1.0 Sol.Frac: 0.188
 k/np/plot: 1 90 znod(nn) 5.728040 Vol1: 0.22924800E+05 U1er: 0.28509817E-09 #setb: 0 #dt: 2881 #itsol: 1
 #CG: 0 #Gauss: 96 #expl: 0 #wet: 96 #chkadvd: 206 #nodneg: 0 #slit: 0



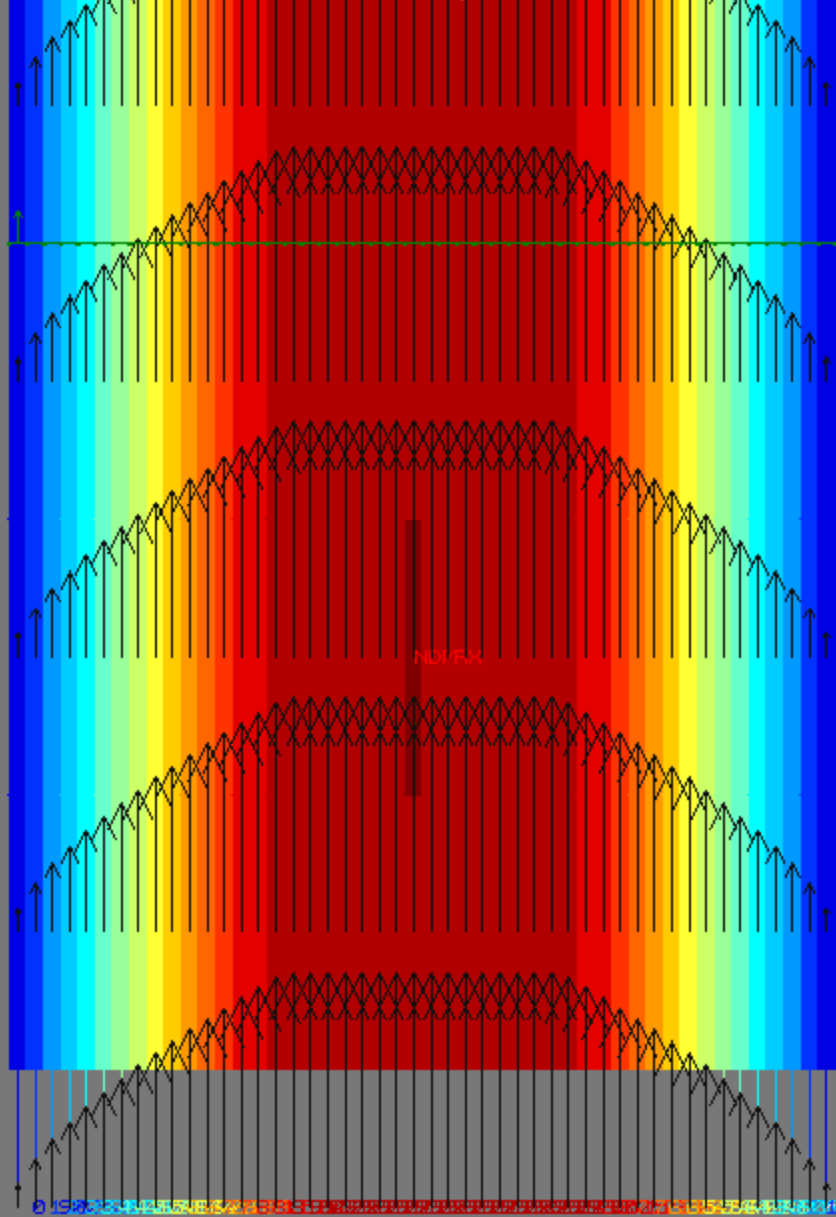
474.264 m³/s

3 cells



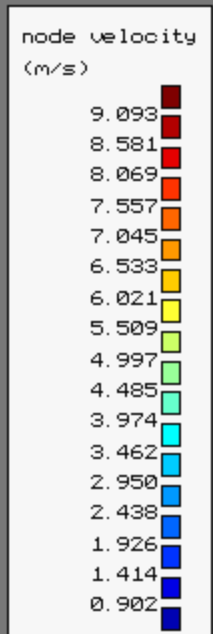
Regular 2D bottom friction approach

TIME S/H/D: 1800.000 0.500 0.021 0.280 H0g.dt: 0.277 CPU/step: 0.015 Tot: 93.3 Sol.Frac: 0.692
 k/rp lot: 90 znod(nn): 1.876464 Udl: 0 15724800E+05 Uler: -.39676029E-08 #setb: 0 #dt: -.6496 #itsol: 5
 #CG: 714 #Gauss: 822 #expl: 0 #uel: 1536 #chk adv: 6814 #nodneg: 0 #slit: 0



509.037 m³/s

48 cells
Q=509 m³/s



Subgrid: Analytic Conveyance approach

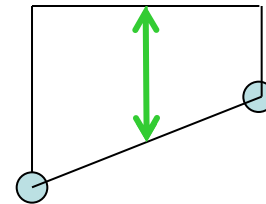
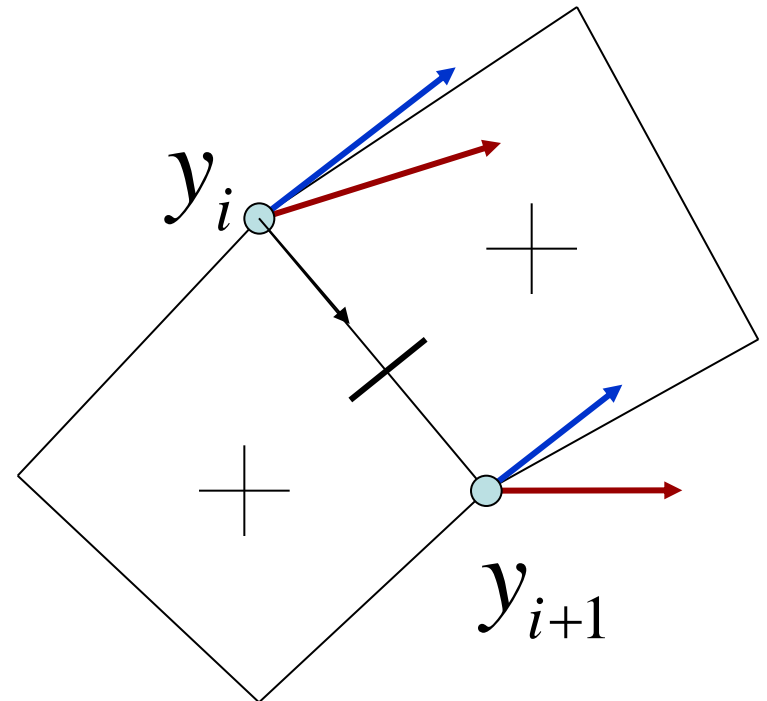
$$\text{friction term: } \frac{uU}{HC^2}$$

$$u = f(y)$$

$$U = g(y)$$

$$H = h(y)$$

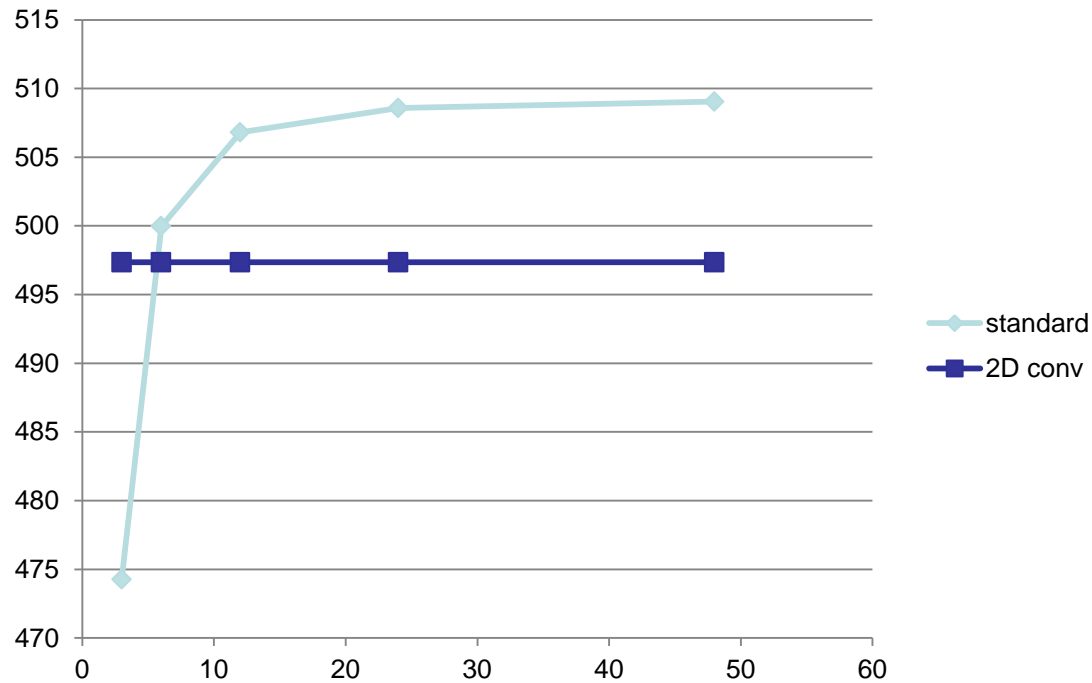
$$C = i(y)$$



Spatial convergence of subgrid approach

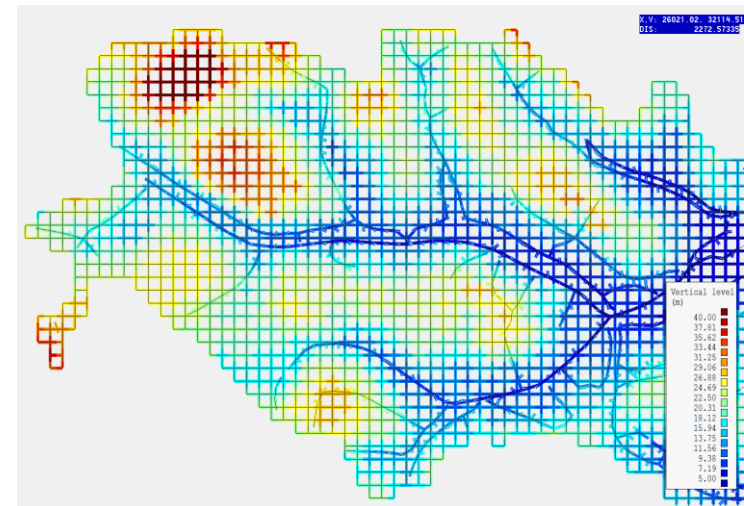


Flooding
Discharge
Capacity
m³/s



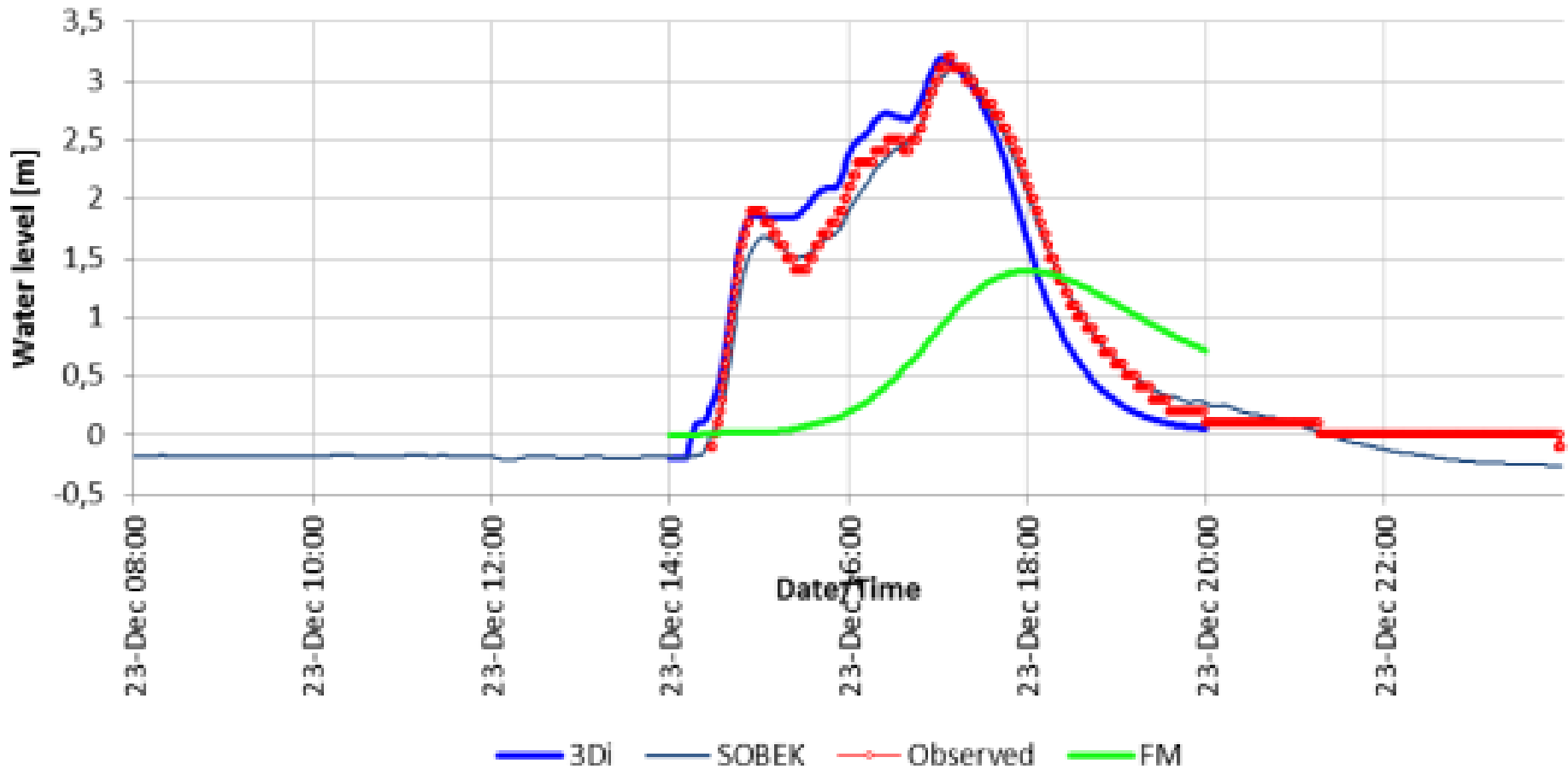
Nr of cells in cross-sectional direction.
3, 6, 12, 24 or 48 cells

Singapore rainfall runoff: Non-linear volumes



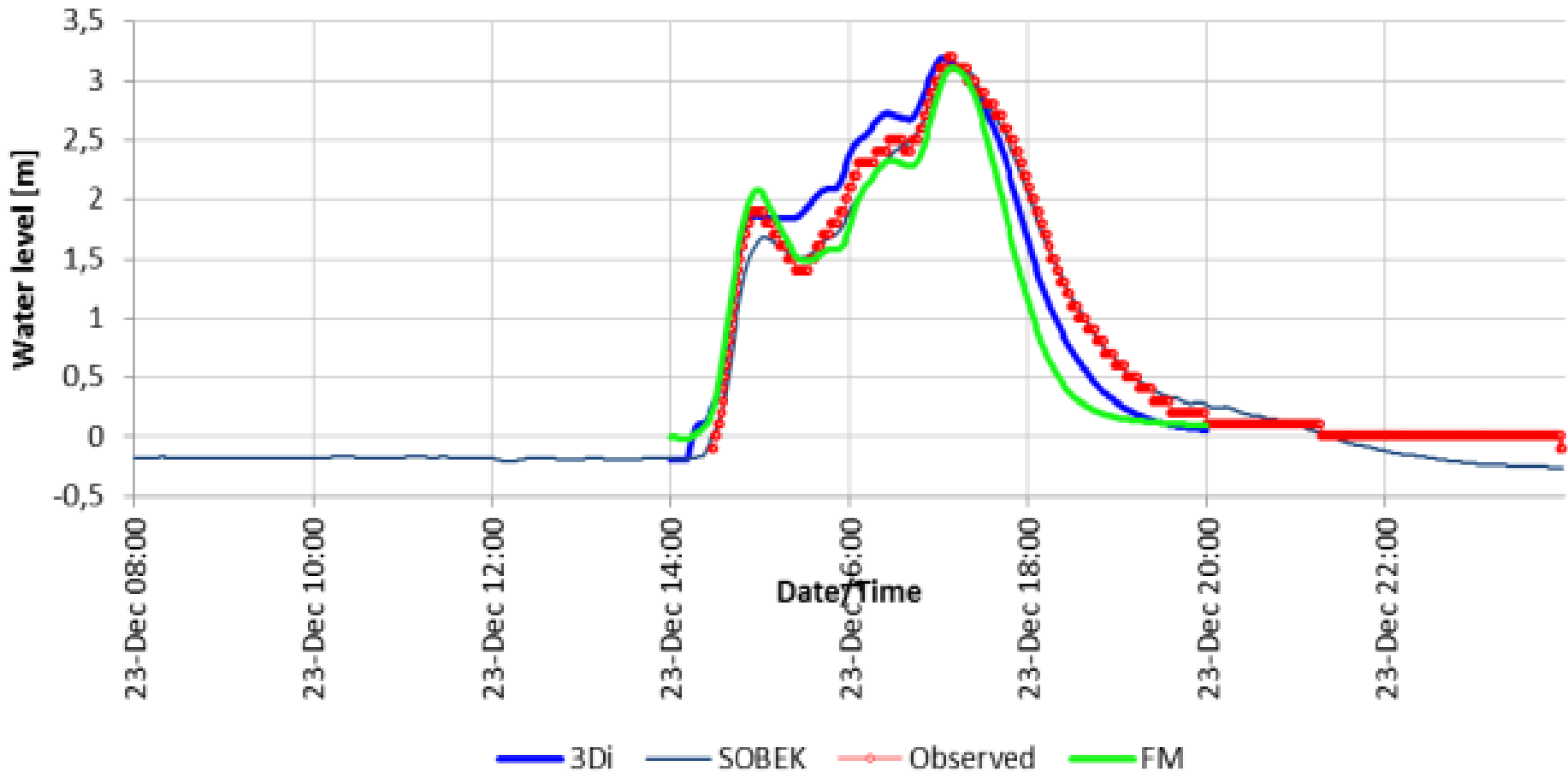
Singapore rainfall runoff: Linear volumes

HMC209 Killiney Rd

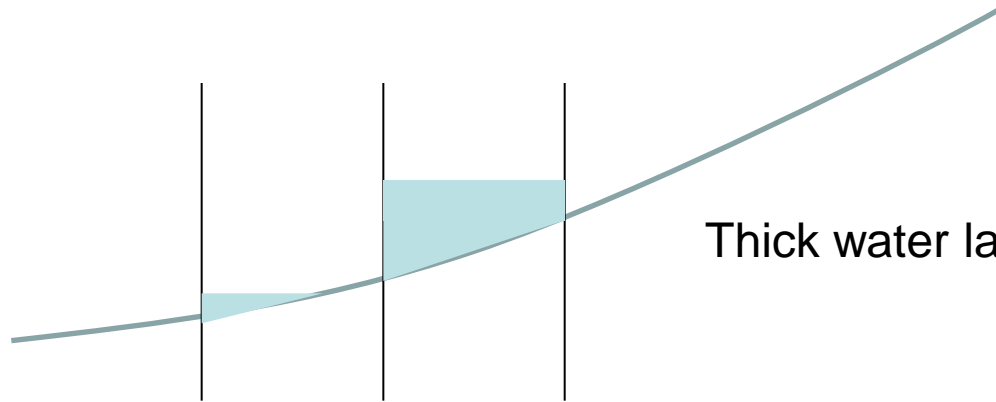
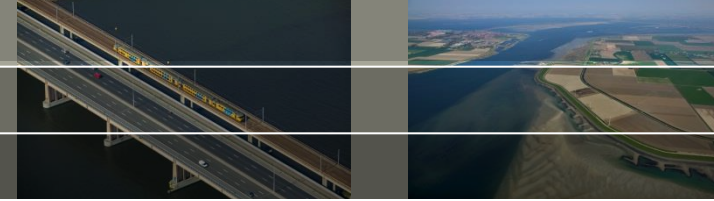


Singapore rainfall runoff: Non-linear volumes

HMC209 Killiney Rd



Subgrid 2: non-linear volumes



Thick water layer : linear volume

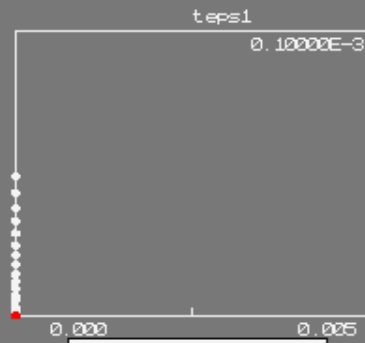
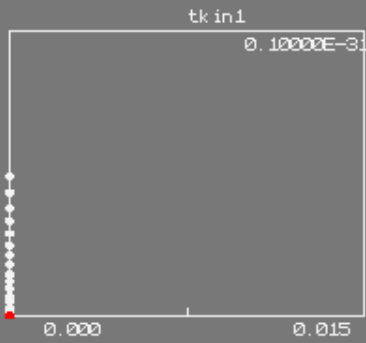
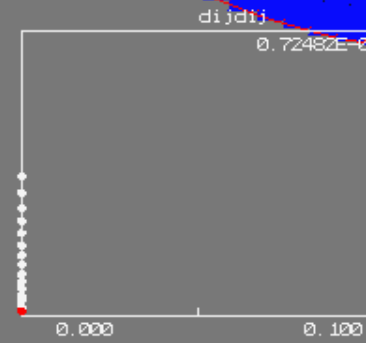
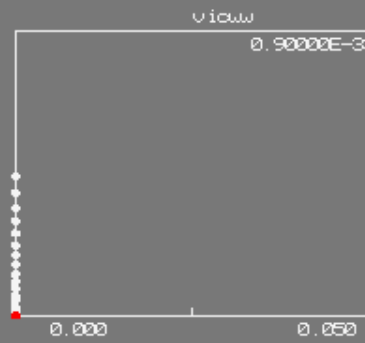
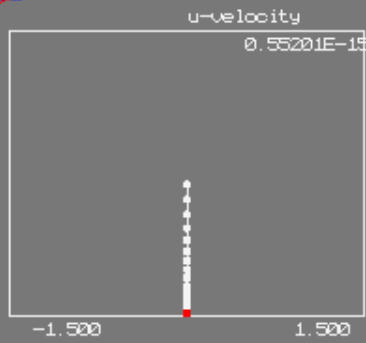
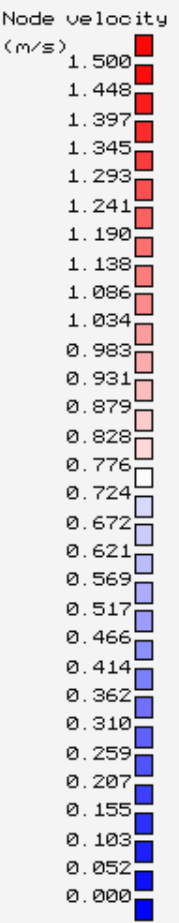
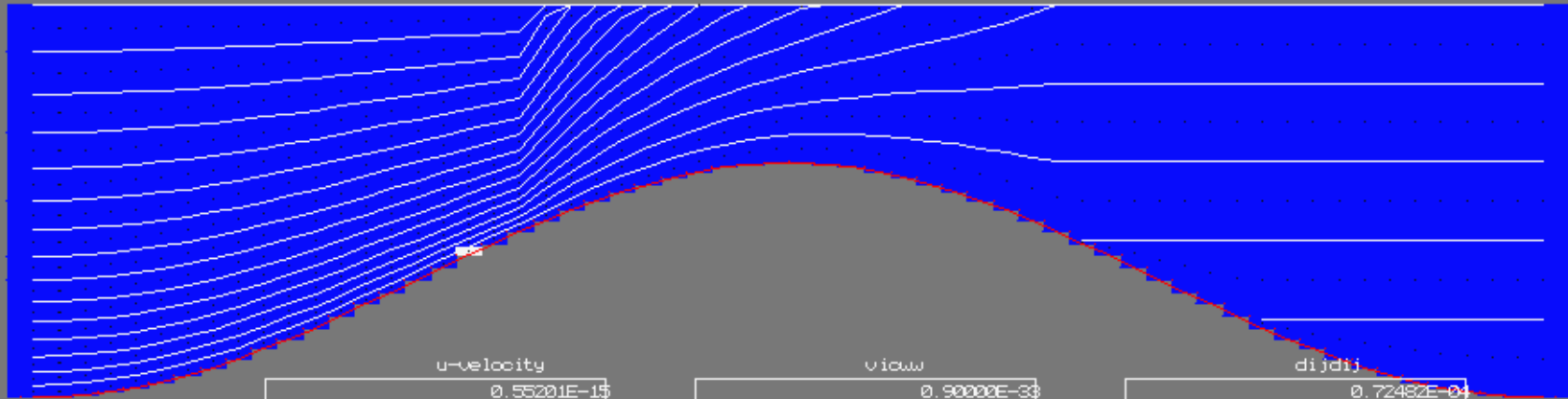
Thin water layer : Non – linear volume

$$V^{p+1} = V^p + (\zeta^{p+1} - \zeta^p) \frac{\partial V^p}{\partial \zeta}$$

$$V^{p+1} = V^p + (\zeta^{p+1} - \zeta^p) A_\zeta^p$$

$$\frac{V^p + (\zeta^{p+1} - \zeta^p) A_\zeta^p - V^n}{\Delta t} + \sum_{out} A_u u - \sum_{in} A_u u = 0$$

Time S/H/D: 3.000 0.001 0.000 dt: 1.000 Avg. dt: 0.750 CPU/step: 0.000 Tot: 0.0 Sol/Rest: 0.000
 k/nplot: 1 18 znod(nn) 0.000000 Uo11: 0.42600247E+05 U1er: 0.24656840E+00 #setb: 0 #dt: 3 #hitsol: 0
 #CG: 0 #Gauss: 62 #expl: 0 #wet: 62 #chkadvd: 0 #nodneg: 0 #slit: 0

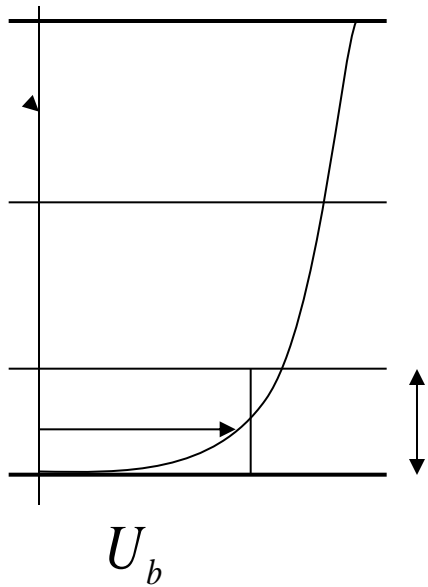


k-eps sanctum

0.000 m3/s

Epsilon b.c. : Neumann
Ustar : Layer integrated

unlike Delft3D
unlike Delft3D



$$u_* = \frac{\kappa U_b}{\ln\left(\frac{\Delta z_b}{2z_0} + 1\right)}, \quad \text{or} \quad u_* = \frac{\kappa U_b}{\ln\left(\frac{\Delta z_b}{ez_0} + 1\right)}$$

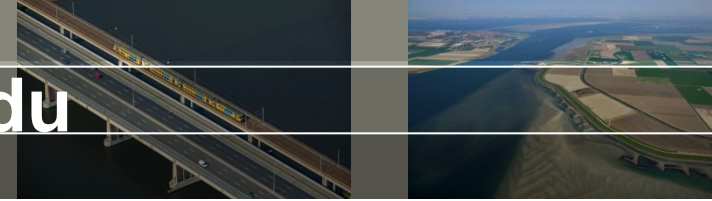
Mid layer

Layer integrated

Delft3D

DFM

Log profile testcase: slope.mdu



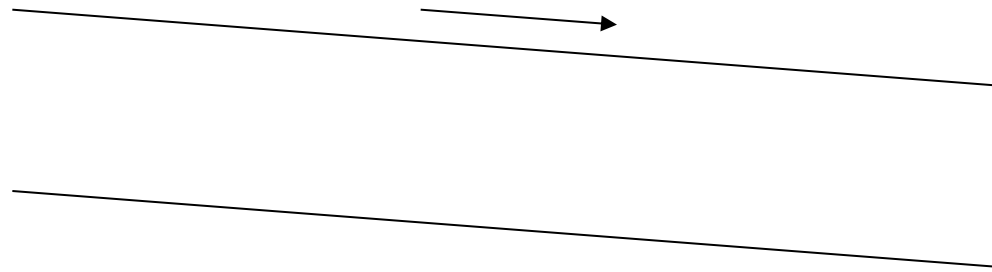
$$L=610 \text{ m}$$

$$Dx=Dy=10 \text{ m}$$

$$i=5e-5$$

$$H=5 \text{ m}$$

$$C=60 \text{ m}^{0.5}/\text{s}$$



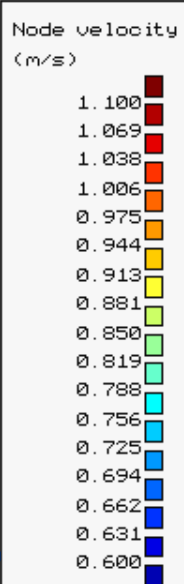
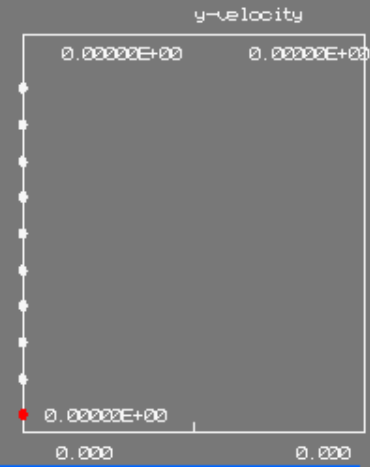
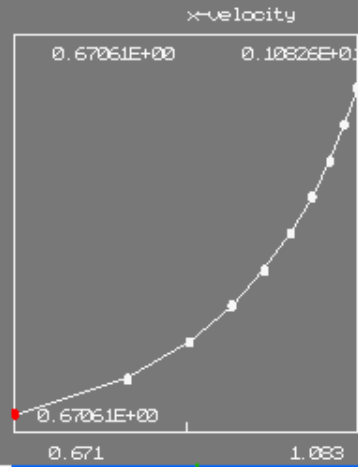
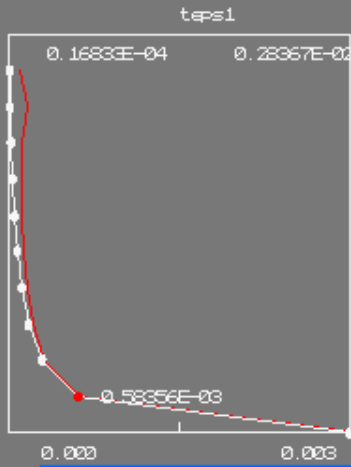
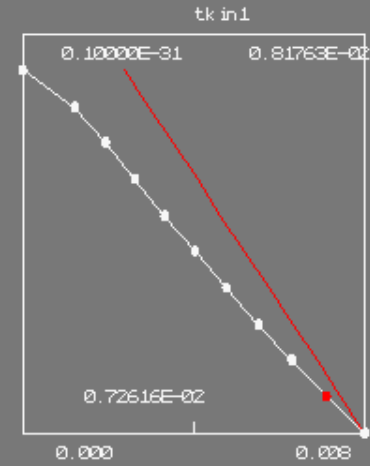
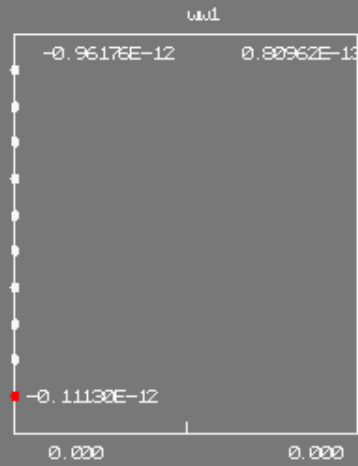
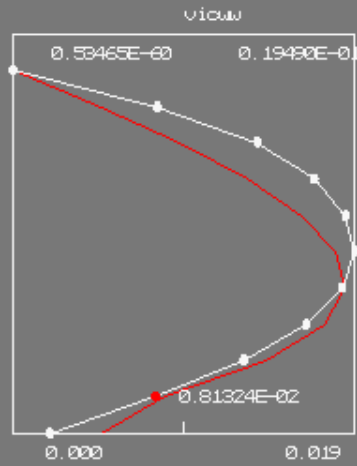
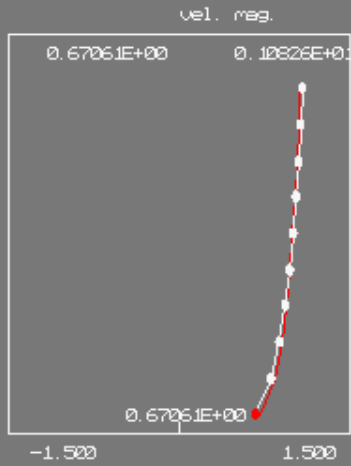
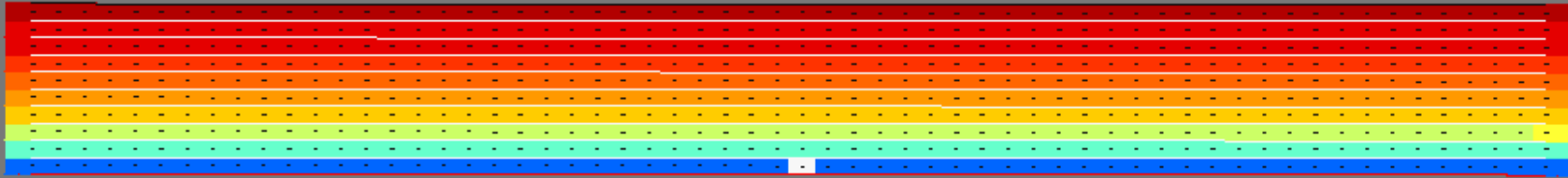
$$U=C(H_i)^{0.5}=0.94868 \text{ m/s}$$

$$Q=47.434 \text{ m}^3/\text{s}$$

K-epsilon sigma 10 layers : 47.466 m3/s

(47.434 m3/s)

0.00E+00
2159 #itsol: 0
slope

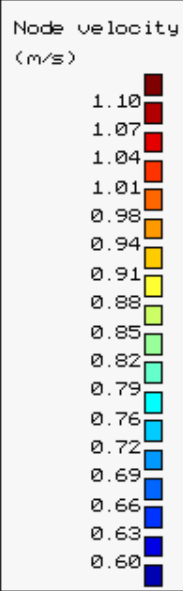
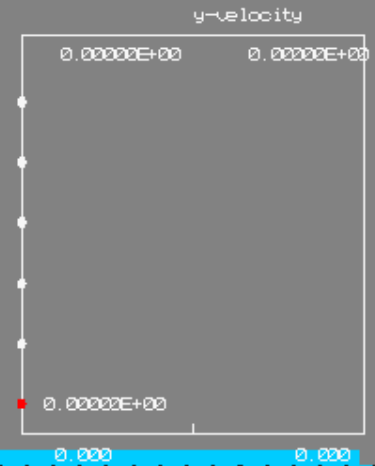
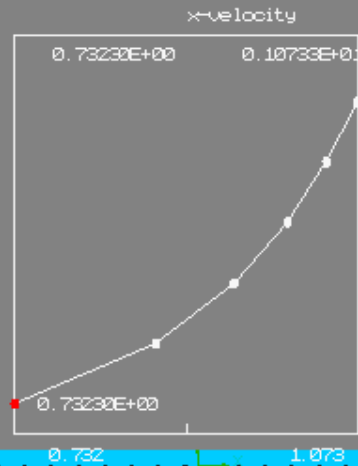
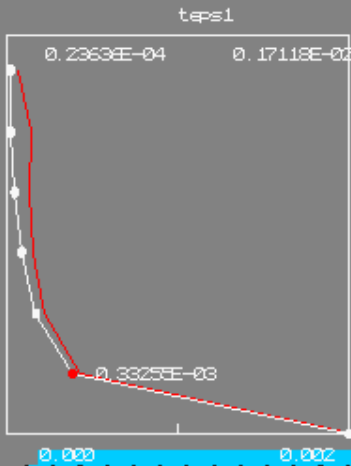
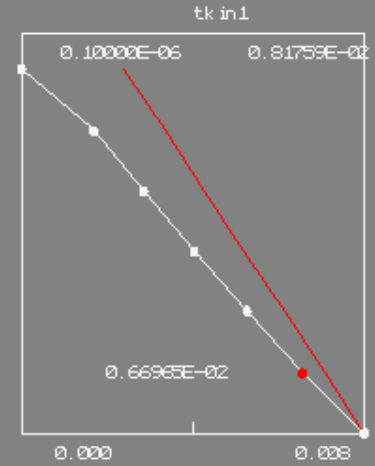
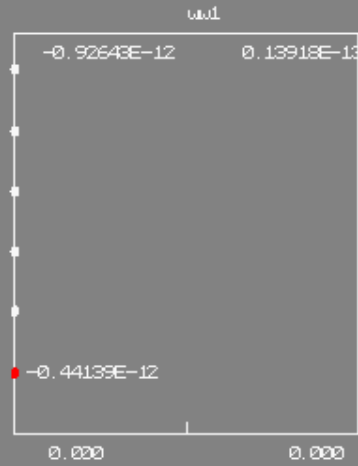
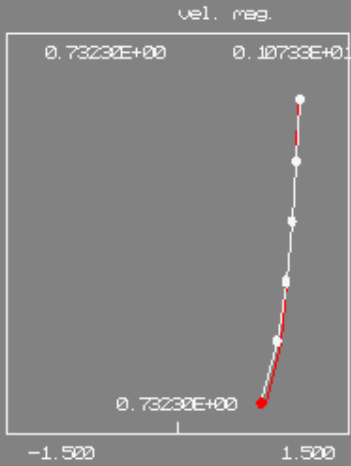
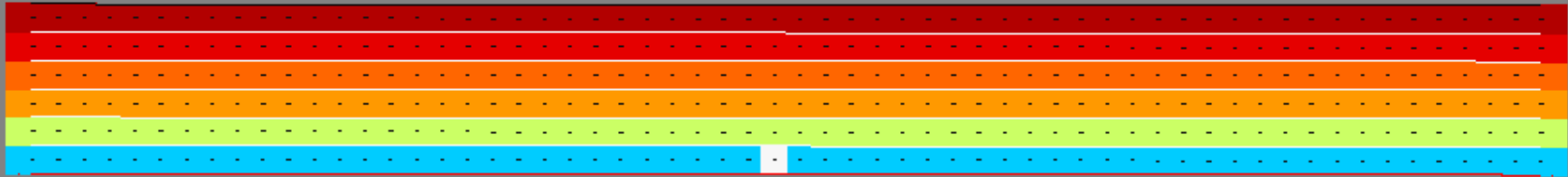


K-epsilon sigma 6 layers : 47.290 m3/s

(47.434 m3/s)

0.000000E+00 Samtot:0.00000000E+00
: 4374 #itsol: 0

#ndx: 62 #Inx: 61 #kmx : 6 #CG: 0 #Gauss: 62 #sllt: 0 iad: 30 5 runid: slope



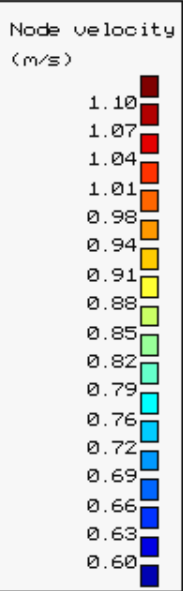
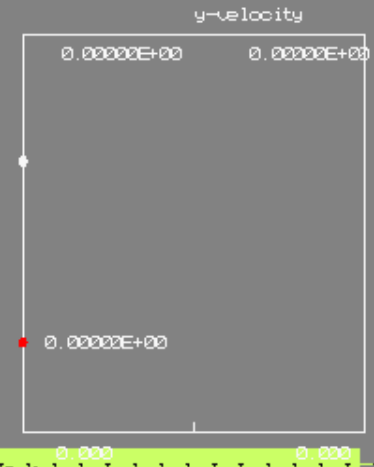
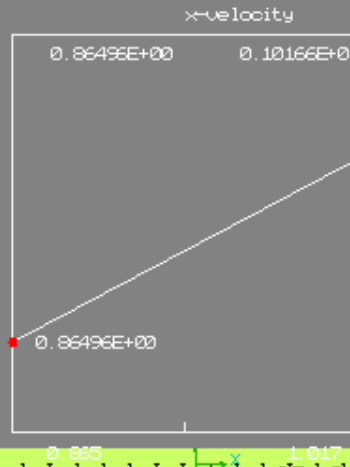
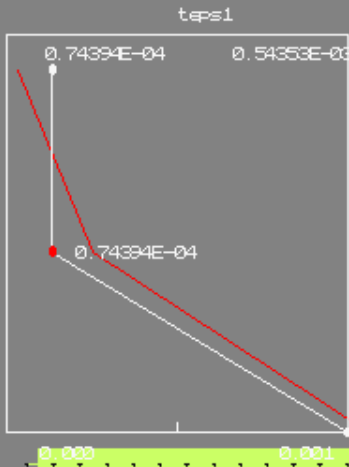
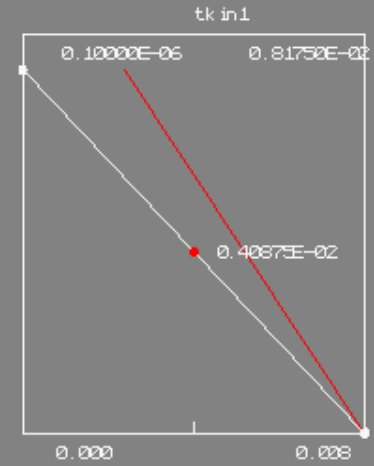
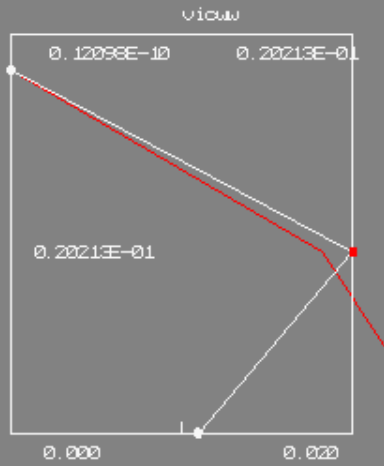
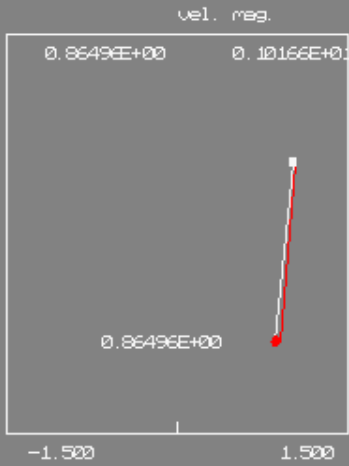
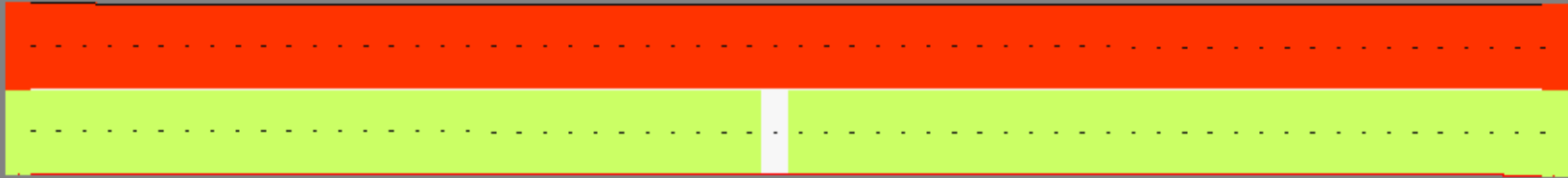
47.290 m3/s

K-epsilon sigma 2 layers : 47.040 m3/s

(47.434 m3/s)

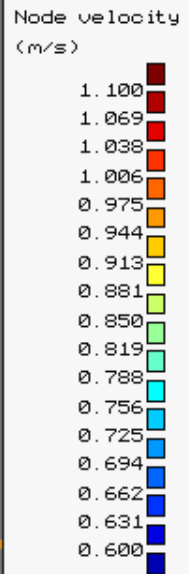
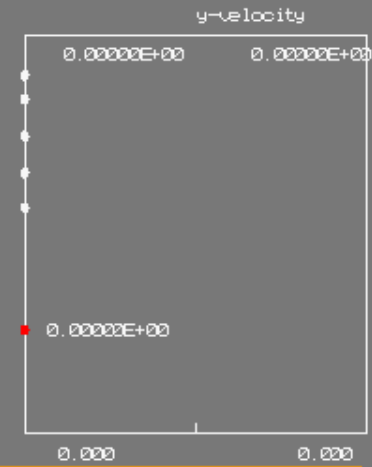
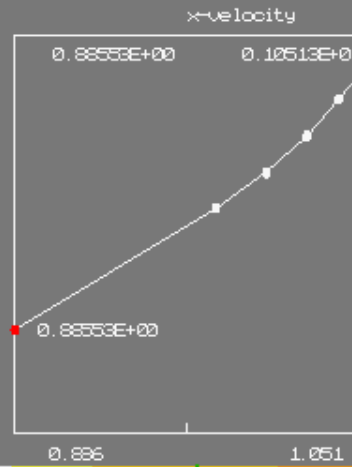
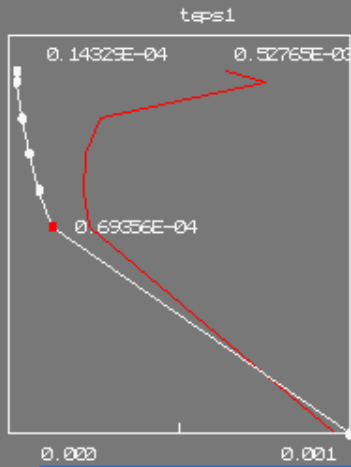
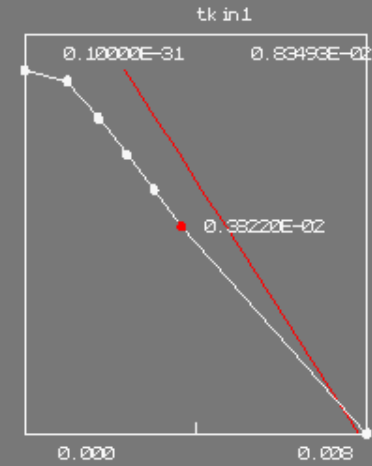
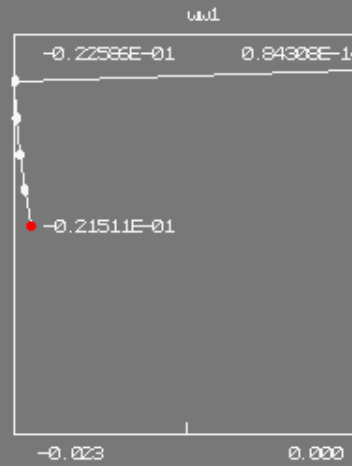
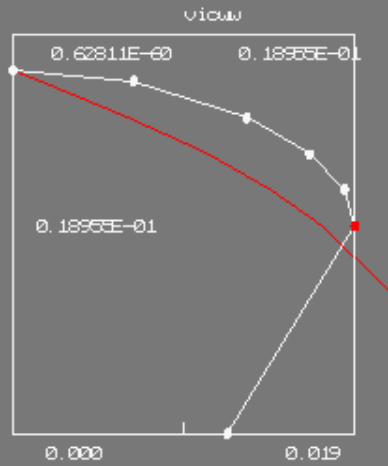
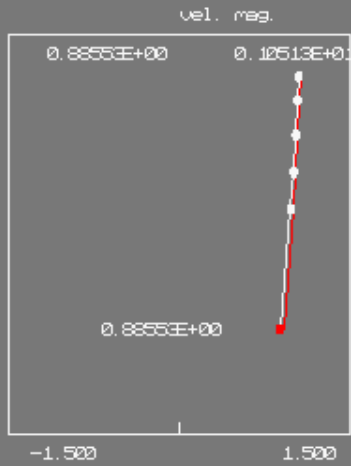
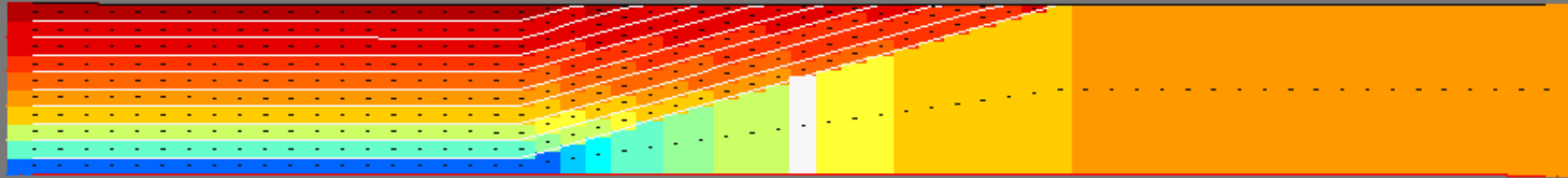
0.000000E+00 Samtot:0.00000000E+00
: 4065 #itsol: 0

#ndx: 62 #Inx: 61 #krx : 2 #CG: 0 #Gauss: 62 #slit: 0 iad: 30 5 runid: slope

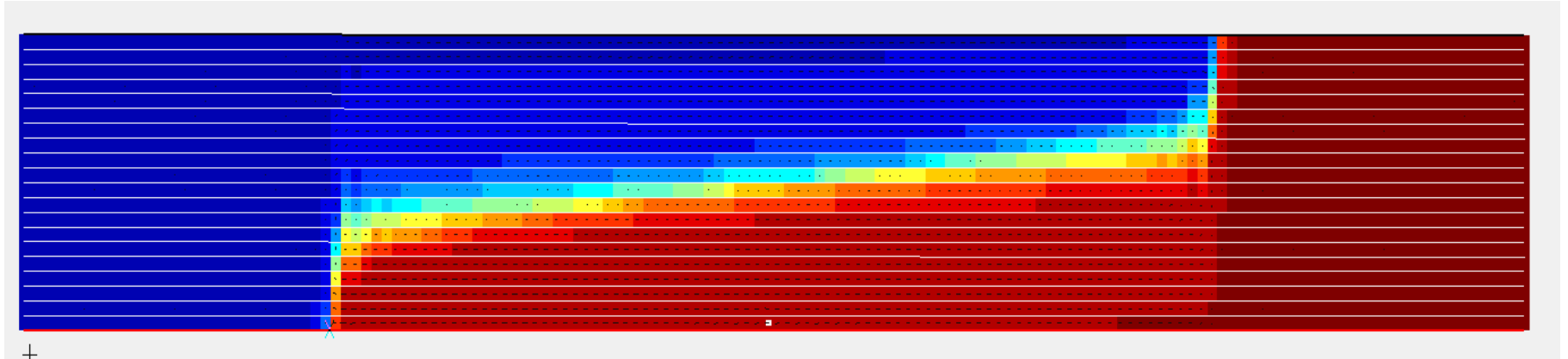
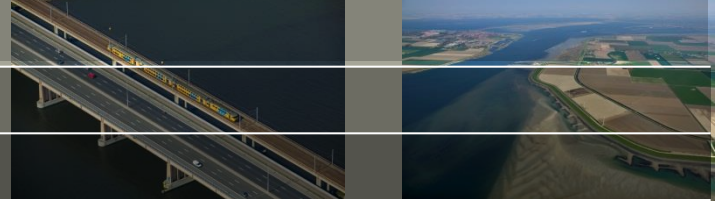


47.040 m3/s

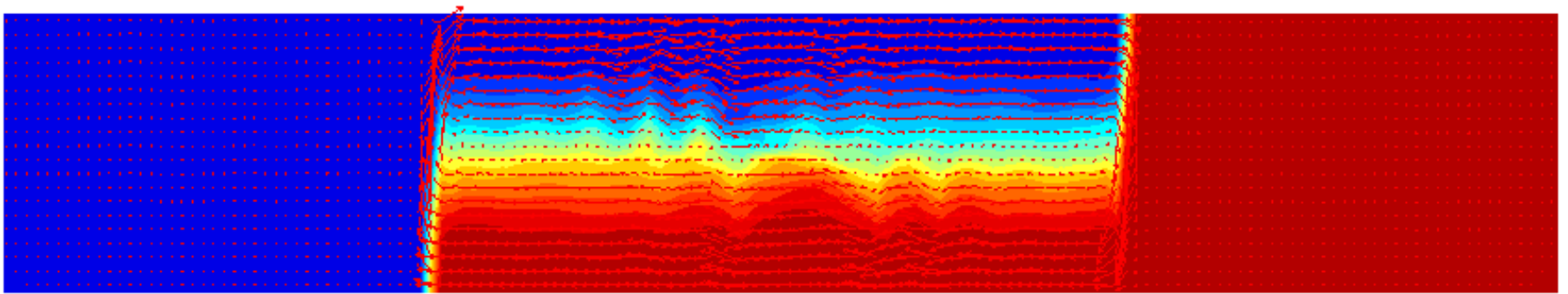
K-epsilon ustar layer integral mixed layers, noadv : $Q = 47.287 \text{ m}^3/\text{s}$ (**47.434** m^3/s)



Lock exchange

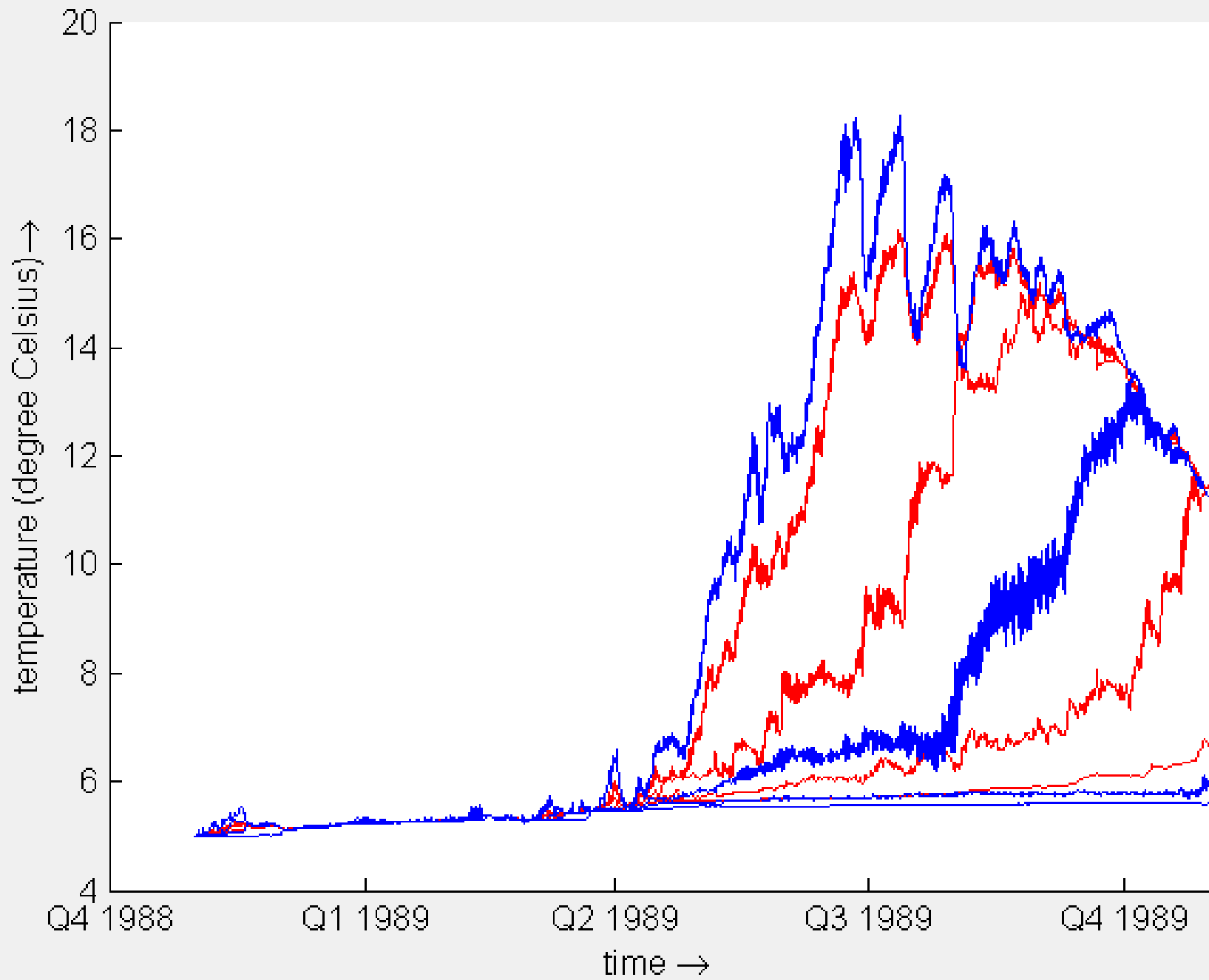


DFM

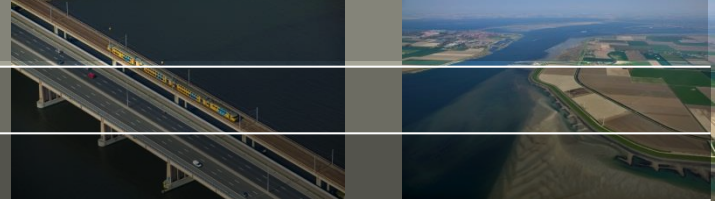


D3D

stat1

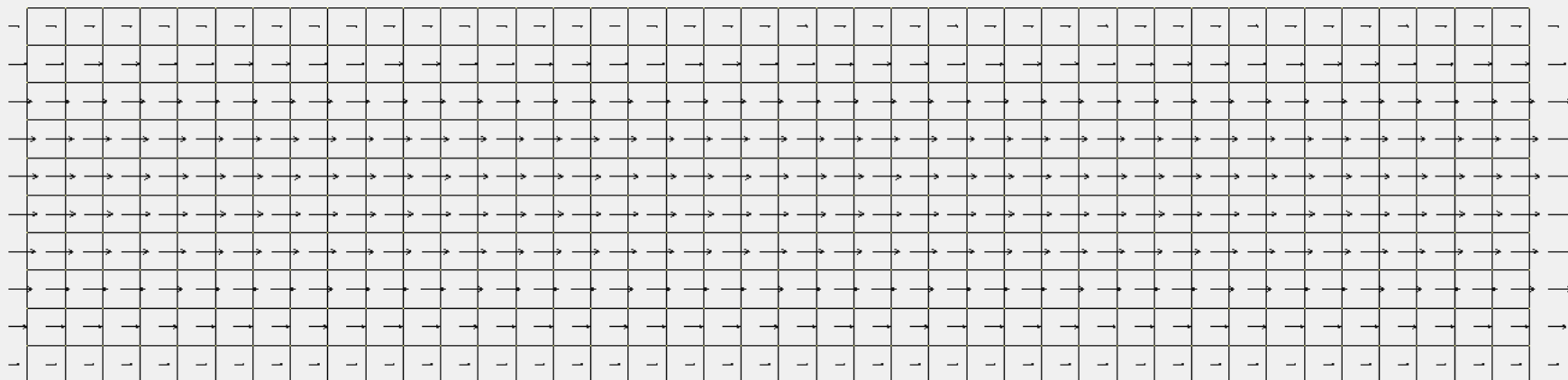
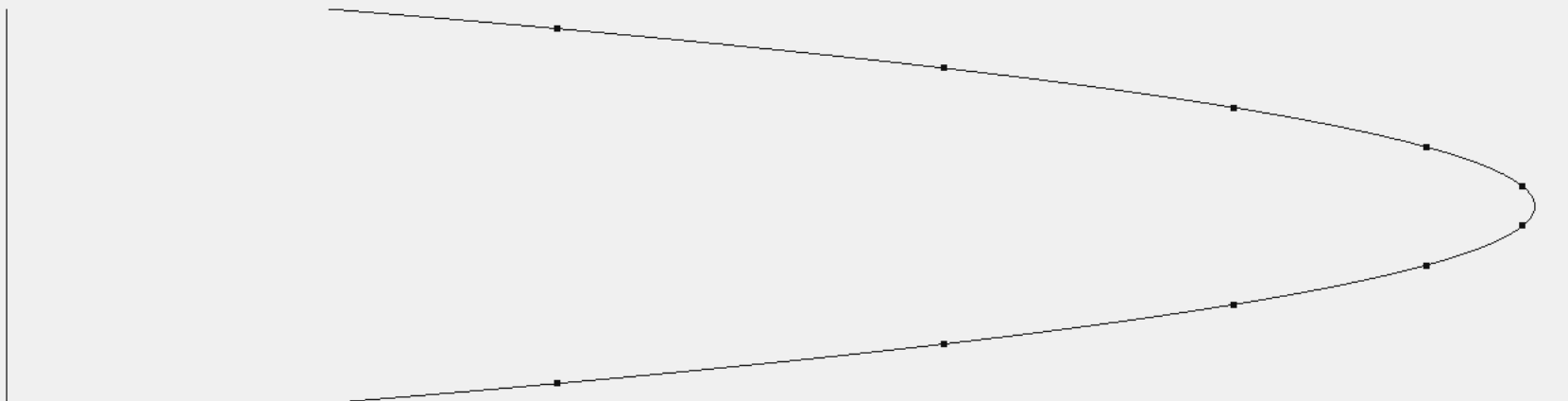


Issues to tackle:



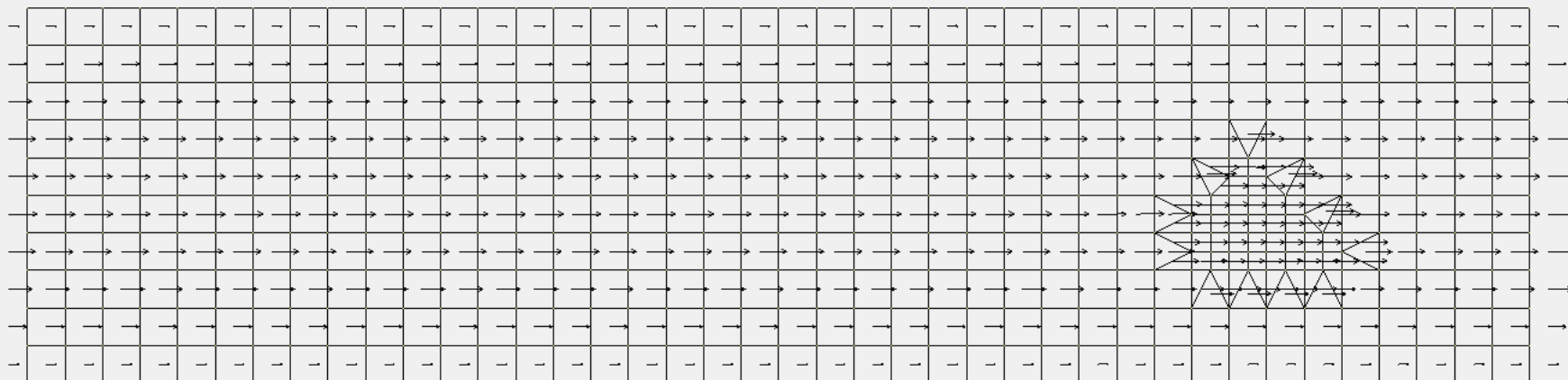
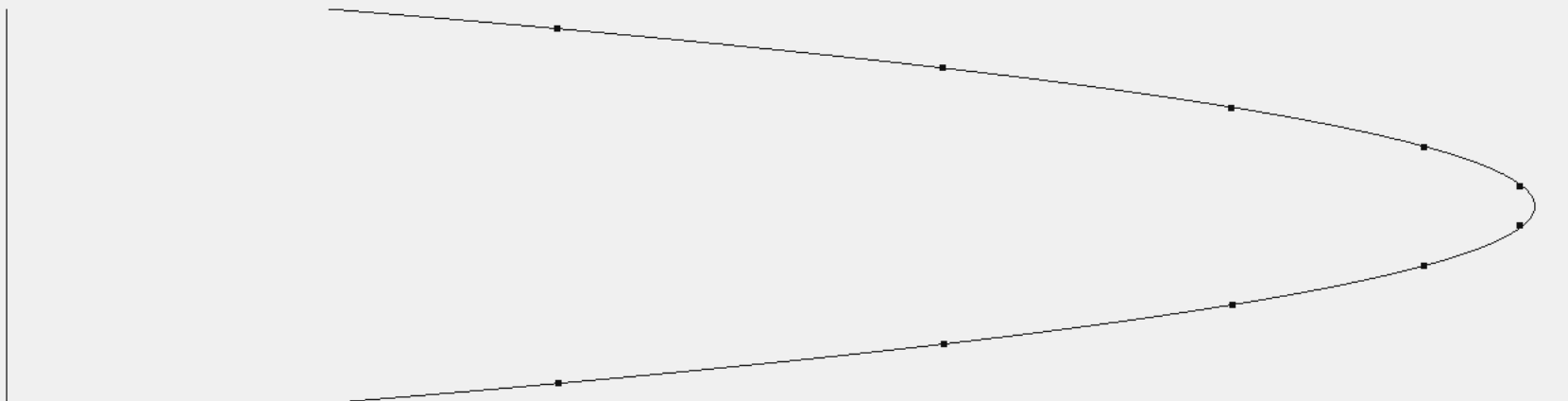
Strongly horizontally sheared flows on irregular grids

19920831 025036 dt: 0.902 Avg.dt: 0.902 CPU/step: 0.000 Tot: 2.4 Sol/Rest:.27E+00 Samer: 0.00000000E+00 Samtot:0.00000000
k/nplot: 1 200 znod(nm): -.99999802E-02 Voll: 0.20000000E+06 Vler: 0.31560828E+00 #setb: 0 #dt: 11344 #itsol: 0
#ndx: 420 #lnx: 770 #kmx: 0 #CG: 180 #Gauss: 240 #slit: 0 iad: 30 5 runid: horvic_partialslip



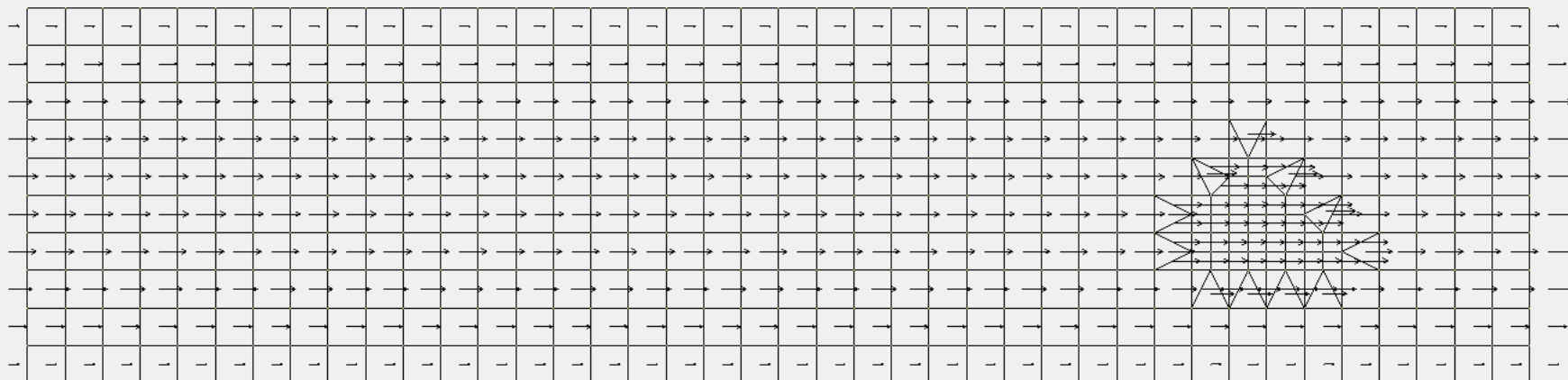
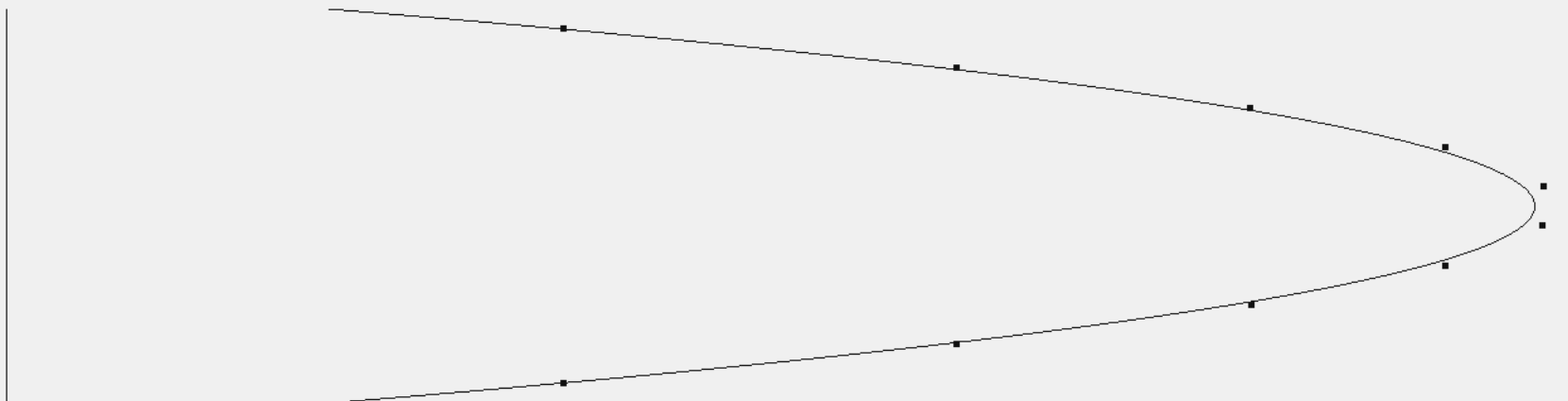
X


```
19920831 040000 dt: 0.227 Avg.dt: 0.227 CPU/step: 0.000 Tot: 14.3 Sol/Rest:.32E+00 Samer: 0.00000000E+00 Samtot:0.00000000
k/nplot: 1 224 znod(nm): -.94805597E-02 Voll: 0.20000043E+06 Vler: 0.31544551E+00 #setb: 0 #dt: 63513 #itsol: 1
#ndx: 469 #lnx: 850 #kmx: 0 #CG: 197 #Gauss: 272 #slit: 0 iad: 0 5 runid: horvic_partialslip
```



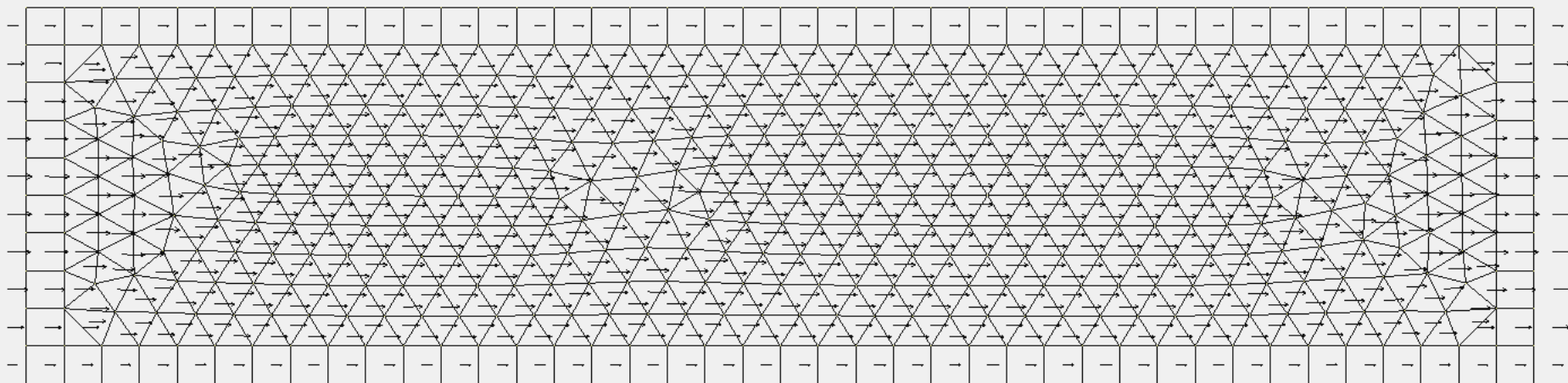
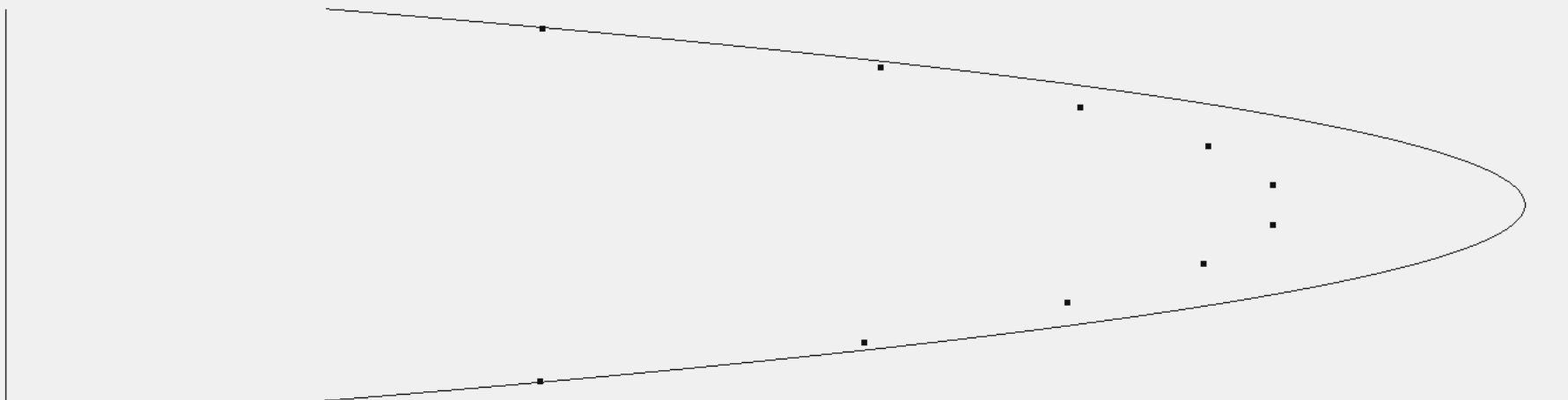
X

```
19920831 040000 dt: 0.224 Avg.dt: 0.225 CPU/step: 0.000 Tot: 15.7 Sol/Rest:.30E+00 Samer: 0.00000000E+00 Samtot:0.00000000
k/nplot: 1 224 znod(nm): -.99837185E-02 Voll: 0.19998605E+06 Vler: 0.31556999E+00 #setb: 0 #dt: 64011 #itsol: 2
#ndx: 469 #lnx: 850 #kmx : 0 #CG: 197 #Gauss: 272 #slit: 0 iad: 330 5 runid: horvic_partialslip
```



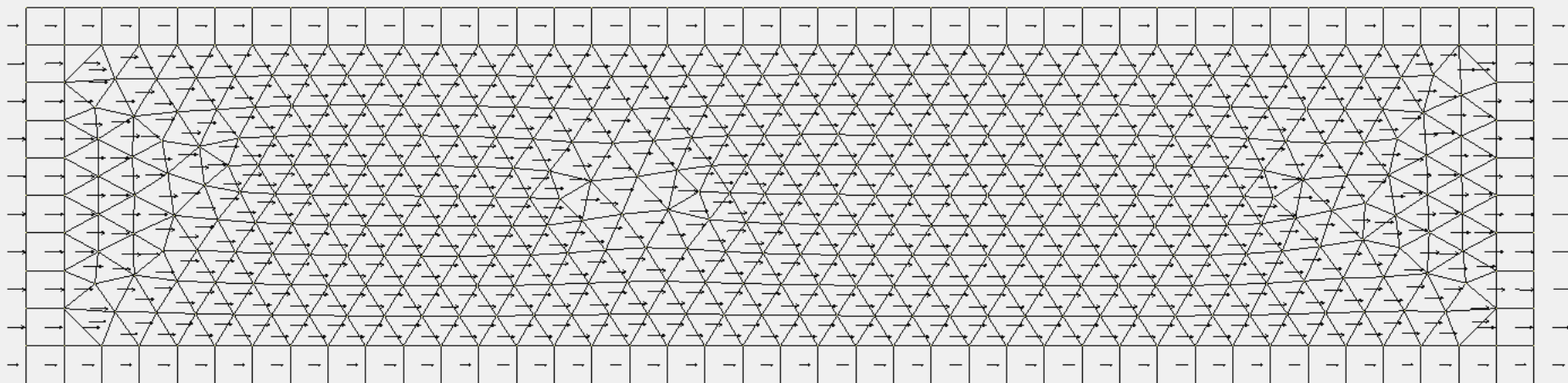
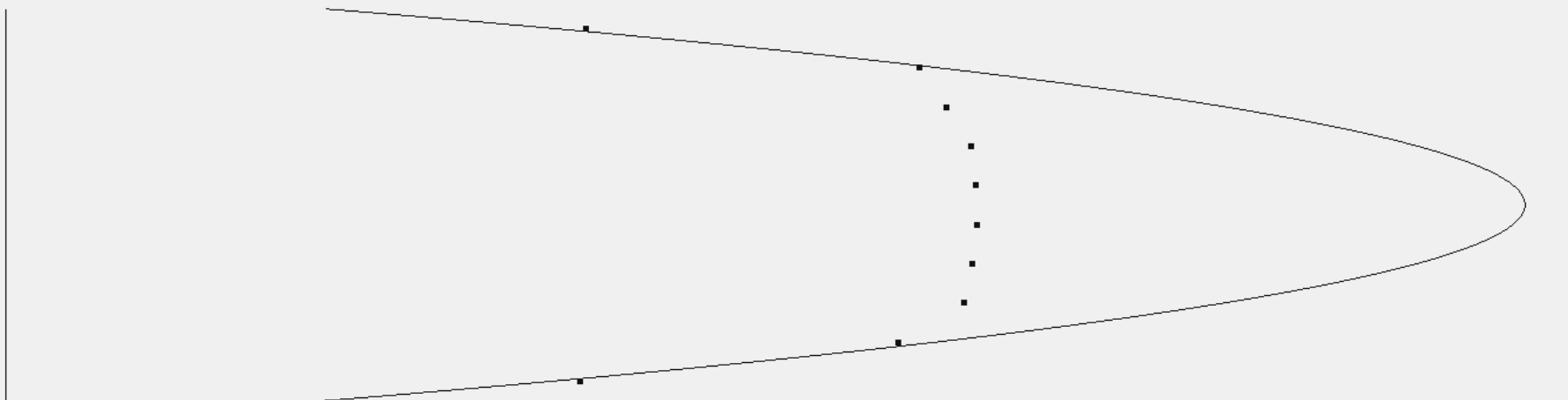
X

```
19920831 060000 dt: 0.375 Avg.dt: 0.355 CPU/step: 0.000 Tot: 20.3 Sol/Rest:.32E+00 Samer: 0.00000000E+00 Samtot:0.00000000
k/nplot: 1 416 znod(nm): -.94721184E-02 Voll: 0.19999918E+06 Vler: 0.37624512E+00 #setb: 0 #dt: 60761 #itsol: 2
#ndx: 852 #lnx: 1266 #kmx : 0 #CG: 297 #Gauss: 555 #slit: 0 iad: 0 5 runid: horvic_partialslip
```



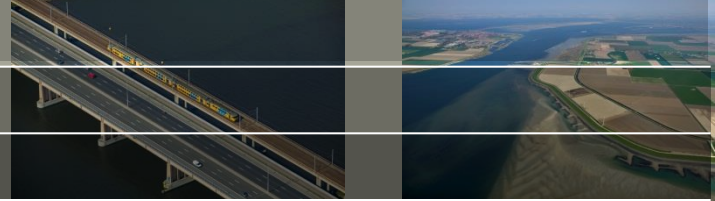
X

```
19920831 060000 dt: 0.486 Avg.dt: 0.455 CPU/step: 0.000 Tot: 17.5 Sol/Rest:.33E+00 Samer: 0.00000000E+00 Samtot:0.00000000
k/nplot: 1 416 znod(nm): -.10819847E-01 Voll: 0.19995671E+06 Vler: 0.46132526E+00 #setb: 0 #dt: 47477 #itsol: 4
#ndx: 852 #lnx: 1266 #kmx : 0 #CG: 297 #Gauss: 555 #slit: 0 iad: 330 5 runid: horvic_partialslip
```



X

Some issues to tackle:

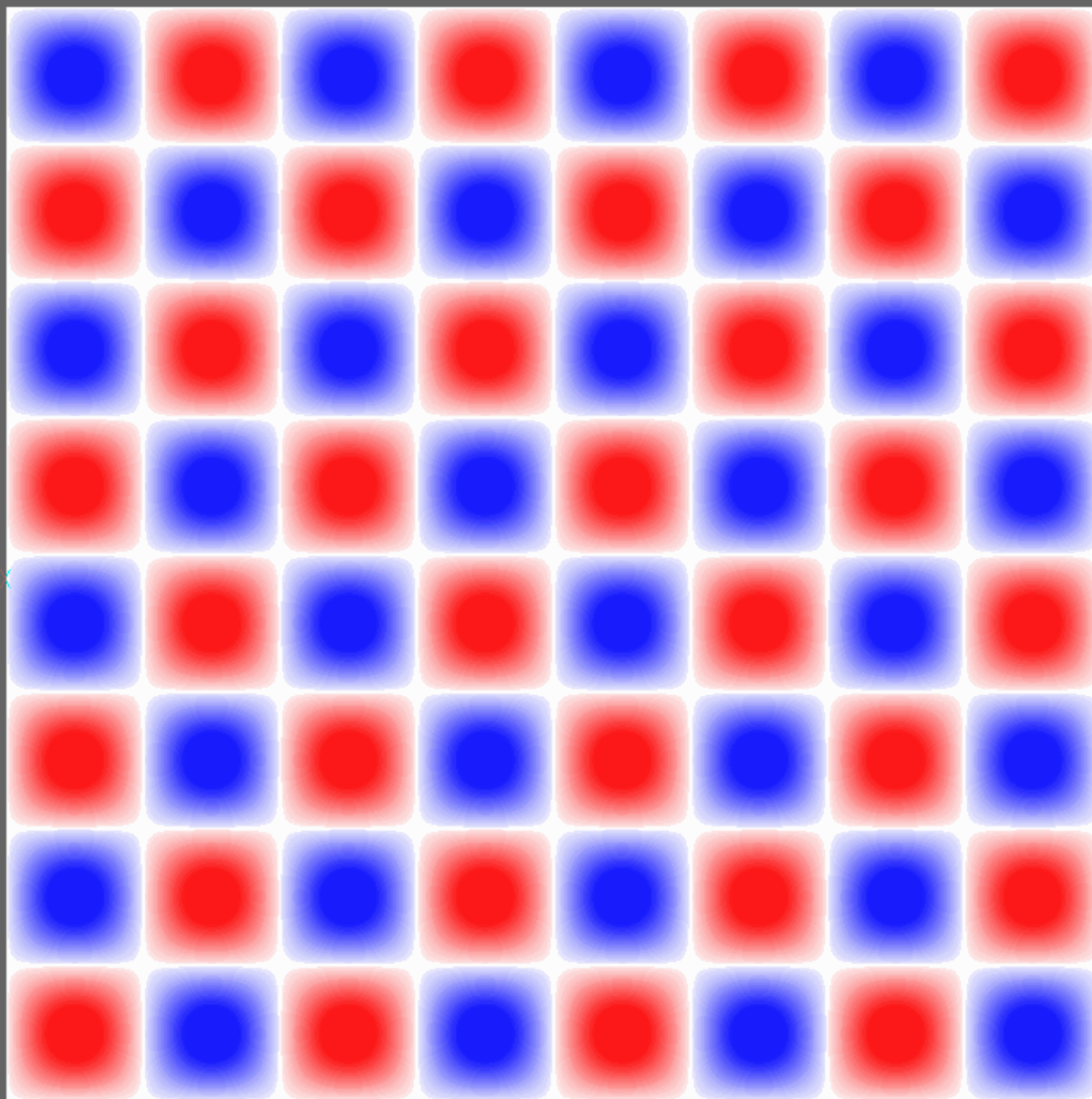


Strongly horizontally sheared flows on irregular grids
(both advection and viscous terms)

Advection in fixed layers

Parallel performance of linear solver (PETSC)

19920831_000001 dt: 0.020 Avg.dt: 0.020 CPU/step: 0.024 Tot: 1.2 Sol/Rest:.76E+00 Samer: 0.00000000E+00 Samtot:0.00000000E+0
k/nplot: 1 20000 znod(nn): -.99900000E+03 Voll: 0.40000001E-01 Vler: -.95062846E-15 #setb: 0 #dt: 50 #itsol: 5
#ndx: 40000 #lnx: 79600 #kmx : 0 #CG: 20080 #Gauss: 19920 #slit: 0 iad: 34 5 runid: checkerboard8



2D vortex merge

